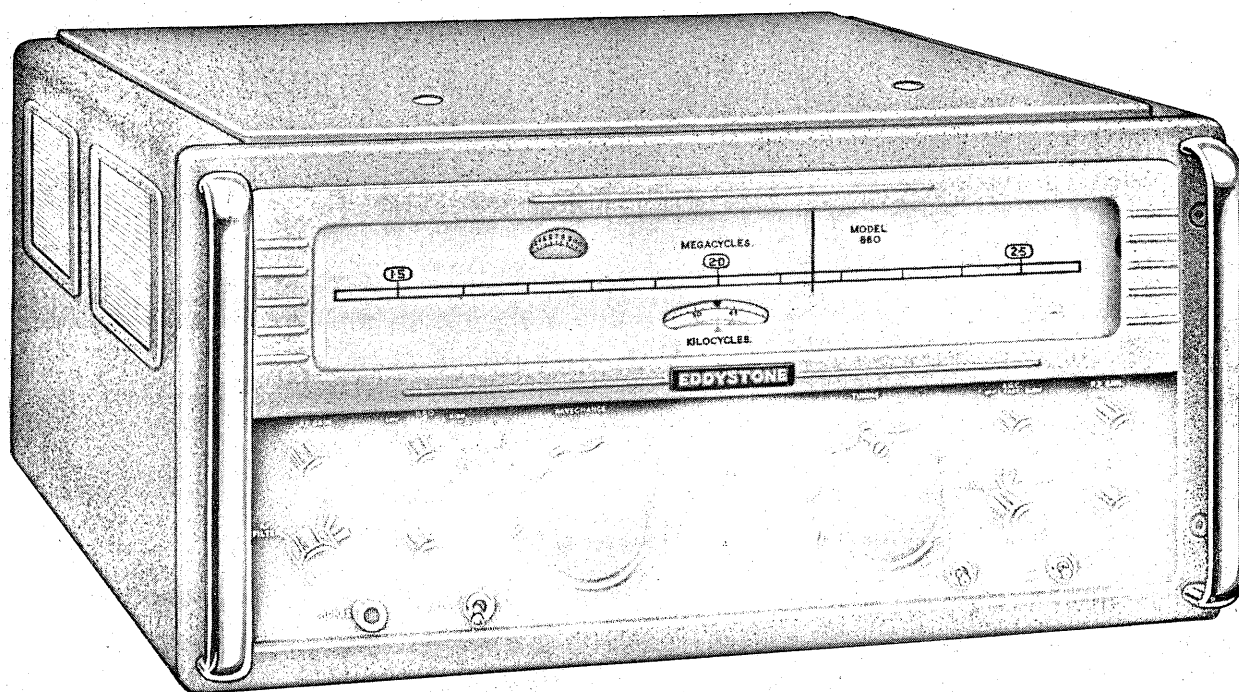




EDDYSTONE

MODEL "S880" HIGH
STABILITY COMMUNICATIONS
RECEIVER

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EDDYSTONE MODEL 'S880'

HIGH STABILITY

COMMUNICATIONS RECEIVER

INTRODUCTION

The EDDYSTONE Model 'S880' is an HF communications receiver of unique design and construction covering the frequency range 500 kc/s to 30.5 Mc/s in thirty switched ranges. Provision is made for the reception of AM, CW and SSB signals and the receiver operates directly from all standard AC mains supplies, or, if these are not available, from any source capable of supplying the necessary HT and LT voltages.

The receiver is exceptionally stable and uses double conversion technique, employing a crystal controlled 1st Local Oscillator and a tuned 'first IF' at all frequencies except those between 2.5-4.5 Mc/s. This band of frequencies coincides with the coverage of the 'first IF' and over this range the receiver functions as a single conversion superhet.

Each of the thirty tuning ranges has a nominal coverage of one Megacycle so giving a constant tuning rate regardless of the range in use. Bandspread is more than adequate for all purposes, the main tuning control requiring no fewer than twenty-four revolutions to cover each range. The presentation of the tuning scale is so arranged that only the calibration applicable to the range in use is visible and the re-setting accuracy is within 1000 c/s at any frequency.

The 'S880' is of robust construction, may be rack or table mounted, and is housed in a strong protective cabinet. All panel controls are conveniently positioned for ease of operation and outputs are available for connection to an external loudspeaker, telephones or remote lines. Provision of a reactance control circuit permits fine tuning of the receiver from a remote listening point, while a 500 kc/s IF output is available for connection to ancillary equipment. A number of receivers may be operated under 'diversity' conditions by linking their AGC lines.

High quality components are employed throughout and the receiver may be used for continuous operation in all areas regardless of climatic conditions.

LIST OF CONTENTS

<u>Section</u>	<u>Page</u>
Introduction .. .	1
List of Contents .. .	2
Technical Information .. .	3
Circuit Description .. .	7
Mechanical Construction .. .	15

ILLUSTRATIONS

Graph of Audio Response in Maximum and Minimum positions of Bass Switch. Fig. 1. .. .	45
Graph of Overall Selectivity with Audio Filter in circuit. Fig. 2. .. .	46
Block Schematic Diagram of Model 'S880'. Fig. 3. .. .	Between Pages 46 & 47
Coupling Arrangements at each position of Selectivity Switch. Fig. 4. .. .	47
Detached Circuit No. 3. .. .	51
Main Circuit Diagram - Parts 1 and 2 .. .	Rear Cover

ABBREVIATION

This publication is made up of extracts from the complete Instruction Manual for the Model 'S880'.

References to diagrams etc., not appearing in this abbreviated Manual should be ignored.

ERRATUM

In Fig. 4. (Page 47), C104a is omitted. Refer to Main Circuit Diagram Part 2 for location.

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TECHNICAL INFORMATION

GENERAL

Frequency Coverage.

The complete coverage is from 500 kc/s to 30.5 Mc/s in thirty switched ranges. Each range has a nominal coverage of 1 Megacycle, but a 100 kc/s overlap is provided at the ends of each range making the actual coverage 1.2 Mc/s.

- Range 1 covers 0.5 - 1.5 Mc/s (nominal)
- Range 30 covers 29.5 - 30.5 Mc/s (nominal)

Intermediate Frequencies.

- 'First IF' - Tuned over the nominal coverage of 2.5-3.5 Mc/s on all 'odd' ranges except Range 1.
Tuned over the nominal coverage of 3.5-4.5 Mc/s on Range 1 and all 'even' ranges.
- 'Second IF' - Fixed tuned to 500 kc/s with variable selectivity. The BFO is adjustable to either side of the pass band by means of a panel control.

Valve Sequence.

A table giving the valves, germanium diodes and silicon rectifiers used in the 'S880' appears on the following page.

Input and Output Impedances.

- Aerial input - 75 ohms (nominal) unbalanced.
- IF output - 75 ohms (nominal) unbalanced.
- AF input - 0.1 Megohm (approx)
- AF output - Loudspeaker: 2.5-3 ohms.
Lines: 600 ohms (balanced or unbalanced).
Telephones: High impedance (nominally 2000 ohms but lower impedances may be used satisfactorily).

Power Supply.

- Mains Operation - 100/125 volts or 200/250 volts AC (40-60c/s).
Consumption 0.37 Amps at 240 volts.
- External Power Supplies - 235 volts at 145 mA for HT
6.3 volts at 6.6 Amps for LT
- Accessory Supplies- When operating from AC mains, the following supplies are available for external use:
HT : 235 volts at 15 mA.
LT : 6.3 volts at 3 Amps.

Power Supply (continued)

Fuses - The live side of the mains input is fused at 1.5 Amps. When operating from external power supplies it is advisable that they are fused at their source.

TABLE 1.

Stage Sequence.

Circuit Ref	Type	Circuit Function
V1	6BA6 (CV454)	1st RF Amplifier.
V2	6BA6 (CV454)	2nd RF Amplifier.
V3	6AK5 (CV850)	1st Mixer.
V4	6BA6 (CV454)	Tuned IF Amplifier.
V5	6AK5 (CV850)	2nd Mixer.
V6	5840* (CV3929)	Crystal Oscillator.
V7	5840* (CV3929)	Buffer/Multiplier. *EF732.
V8A	6U8	Reactance Control Valve.
V8B		Variable Frequency Oscillator.
V9	6C4 (CV133)	Buffer.
V10	6BA6 (CV454)	1st 500 kc/s IF Amplifier.
V11	6BA6 (CV454)	2nd 500 kc/s IF Amplifier.
V12	6BA6 (CV454)	3rd 500 kc/s IF Amplifier.
V21	6489 (CV469)	AM Detector.
V13A		Noise Limiter.
V13B	6AL5 (CV140)	AGC Rectifier.
V14A		Cathode Follower (IF Output).
V14B	12AT7 (CV455)	Cathode Follower (CW/SSB Detector).
V15A		Meter Control Valve.
V15B	12AT7 (CV455)	AF Amplifier.
V16	6BE6 (CV453)	CW/SSB Detector.
V17A		AF Amplifier.
V17B	12AU7 (CV491)	Phase Splitter.
V18	6AM5 (CV136)	
V19	6AM5 (CV136)	Push-pull AF Output.
V20	OB2 (CV1833)	Voltage Stabiliser.
D1-D4	DDO06 (FST1/4)	HT Rectifier. (silicon diodes)

PERFORMANCE

Sensitivity.

At frequencies below 10 mc/s, better than 5 microvolts for an output of 50 milliwatts with a signal modulated to a depth of 30% (400 c/s) and a signal-to-noise ratio of 15dB. At all other frequencies the sensitivity is better than 3 microvolts and the CW sensitivity is of the order of 1 microvolt at all frequencies.

Selectivity.

Five degrees of overall selectivity are provided, namely:

'BROAD'	'CRYSTAL'
'INTERMEDIATE'	'CRYSTAL WITH AUDIO FILTER'
'NARROW'	

Typical response figures for the 'BROAD', 'NARROW' and 'CRYSTAL' positions are as follows:

'BROAD'	: 6dB down at 7 kc/s off resonance. 30dB down at 13 kc/s off resonance.
'NARROW'	: 6dB down at 1.5 kc/s off resonance. 30dB down at 4 kc/s off resonance.
'CRYSTAL'	: 6dB down at 200 c/s off resonance. 30dB down at 2 kc/s off resonance.

Stability.

Thermal.

At any frequency, drift does not exceed 100 c/s in 1 hour after a 2 hour 'warm-up' period.

Long term drift with temperature changes of up to 20° C. is not greater than 50 c/s.

Mains Voltage Variation.

A variation of + 10% in the applied mains voltage does not affect the frequency stability by more than + 100 c/s.

Image Rejection.

Rejection of all images is greater than -70dB at signal frequencies above 15 Mc/s, rising to greater than -90dB below 15 Mc/s.

IF Rejection.

Greater than -90dB on all ranges except Range 1. Rejection on Range 1 is greater than -60dB.

Calibration and Re-setting Accuracy.

Within 1000 c/s at all frequencies.

Noise Factor.

Ranges 2 - 30	 5dB (?)
Range 1	 Noise figure measurements not reliable in this range.

Cross Modulation.

With a desired signal 60dB above 1 uV, the interference produced by a signal 10 kc/s 'off-tune' and of strength 90dB above 1 uV will be 30dB below the output of the desired signal.

Intermodulation.

Two signals whose sum or difference frequency is equal to either the Intermediate Frequency or the selected Signal Frequency, must each be of a level greater than 100dB above 1 uV to produce an output equal to that produced by a normal signal 20dB above 1 uV.

Blocking.

With a desired signal 60dB above 1 uV, an interfering carrier 10 kc/s 'off-tune', has to be of a level exceeding 90dB above 1 uV to affect the output by 3dB.

AGC.

With AGC in operation, the audio output level does not change by more than 6dB for a carrier variation of 100dB above 3 uV.

The AGC time constants are as follows:

AGC 'FAST' : 0.025 sec. AGC 'SLOW' : 0.25 sec.

AGC is available for diversity reception if required. (terminal at rear of set.)

Audio Output and Response.

The push-pull AF Output Stage will deliver up to 2 watts of audio power to a 2.5 ohm loudspeaker.

The audio response depends on the position of the Bass Switch and whether the Audio Filter is in or out of circuit. Graphs at the rear of this manual show the response of the Audio Section with the Audio Filter switched out (Fig.1.), and the overall receiver selectivity with the Audio Filter in circuit (Fig.2.).

Distortion.

For an output of 1 watt : 5% , 2 watts : 10%

Hum Level.

Better than -50dB below 1 watt.

IF Output.

With AGC in use, an output of 100 millivolts is obtained for an input signal of 5 uV.

A maximum output of 300 mV is available with AGC 'OFF'.

Radiation.

No radiation from the receiver exceeds 5 uV into 75 ohms.

Remote Frequency Control.

Average rate of freq. change - 1 kc/s for 2 volts applied.

CIRCUIT DESCRIPTION

PRINCIPLE OF TUNING EMPLOYED IN THE 'S880'

Before considering the complete circuit in detail, it will be advantageous to the user to have a knowledge of the somewhat unusual method of tuning used in the 'S880'. The IF/AF Section will be dealt with first, since, in addition to being the simpler portion of the receiver, a knowledge of its operation is helpful in understanding the more unconventional RF Section.

Reference to Fig.3. will show that the IF/AF Section (V4 etc.) is in effect, a single conversion superhet having two switched tuning ranges, the range switching and tuning being ganged to the corresponding controls in the RF Section. On all the 'odd' RF ranges except Range 1, the IF Section tunes from 2.5-3.5 Mc/s but changes over to 3.5-4.5 Mc/s on Range 1 and all the 'even' RF ranges. The two IF ranges will be known as Ranges 'A' and 'B' respectively.

The Local Oscillator associated with the IF Section always tunes the range 3.0-4.0 Mc/s, tracking 500 kc/s high on Range 'A' and 500 kc/s low on Range 'B' resulting in a constant difference frequency of 500 kc/s appearing in the output from the Mixer Stage (V5). This IF output is applied to a conventional three stage IF amplifier feeding the later stages in the receiver.

The tuning of the IF Section is arranged so that regardless of the RF range in use, the 'tuned' IF will be set to its highest frequency when the tuning pointer lies at the left hand end of the tuning scale. This of course, is the reverse of normal practice, where the highest frequency usually occurs at the right hand end of the scale. The reason for arranging the tuning in this way will be made clear later when dealing with the RF Section.

The RF tuning of the 'S880' covers the band 500 kc/s to 30.5 Mc/s in thirty 'one Megacycle ranges', two of which, Ranges 3 and 4, coincide with the two ranges of the tuned IF. On these ranges the receiver functions as a single conversion superhet, the tuned IF Stage becoming an RF Stage since it operates at the same frequency as the incoming signal. Fig.3. shows that the tuned IF Stage is preceded by the 1st Mixer and this also functions as an RF amplifier on Ranges 3 and 4, its Local Oscillator being rendered inoperative by the range switching. The two RF Stages, V1 and V2, operate normally, so that the receiver has a total of four stages of RF amplification when used as a single conversion superhet. All the four stages are gang tuned, the direction of tuning being dictated by that employed in the IF Section, namely frequency increasing from right to left on the tuning scale. On all other ranges the scale calibration follows normal practice with frequency increasing from left to right.

On frequencies other than those in the band 2.5-4.5 Mc/s, the receiver becomes a double conversion superhet having two tuned RF Stages, a crystal controlled 1st Local Oscillator and a tuned 'first IF'. The injection frequency from the 1st Local Oscillator is so arranged that

when tuning any one of the F ranges (other than Ranges 3 and 4), the output from the 1st Mixer will lie in one of the ranges covered by the tuned IF stage.

Taking as an example the RF range covering 10.5-11.5 Mc/s. Injection from the 1st Local Oscillator is at 14 Mc/s resulting in an IF output of 3.5 Mc/s for a signal at 10.5 Mc/s and 2.5 Mc/s for an 11.5 Mc/s signal. It will be noted that the highest frequency in the RF range produces the lowest frequency in the IF range, and it is for this reason that the IF tuning is in the reverse direction to normal. The RF tuning is arranged (as is the scale calibration) to increase in frequency with pointer movement from left to right.

On the next range lower, 9.5-10.5 Mc/s, the same injection frequency is employed, but since the RF range is removed one Megacycle further from the crystal frequency, the IF output will be one Megacycle higher, i.e. 3.5-4.5 Mc/s.

On the range above 10.5-11.5 Mc/s, the crystal is changed by the range switching to produce an injection frequency of 16 Mc/s. At the LF end of the range (11.5 Mc/s), the IF output becomes 4.5 Mc/s, while a signal at 12.5 Mc/s produces output from the 1st Mixer at 3.5 Mc/s.

The same crystal (16 Mc/s) is used on the next range higher, producing an IF output in the lower of the two IF ranges (Range 'A').

Careful study of Table 2 will provide a complete picture of the technique adopted in covering the entire tuning range of the '8880'. In general, one crystal serves for two adjacent ranges (one 'odd' and one 'even'), the 'first IF' alternating between Range 'A' and 'B'. On certain ranges these 'rules' do not apply but this is made clear in the table.

It should be noted that each range is adjusted and calibrated to cover a little more than the figures given in the table. To provide an overlap between adjacent ranges, each range tunes 100 kc/s outside the limits quoted. The same applies to the tuned IF which covers either 2.4-3.6 Mc/s or 3.4-4.6 Mc/s depending on the RF range in use. A coverage of exactly one Megacycle per range was assumed in order to simplify both the explanation above and the table which follows.

THE RF SECTION

This comprises two stages of RF amplification together with the 1st Mixer Stage and its associated Local Oscillator Unit.

The two RF Stages, V1 and V2, employ high slope vari-mu RF pentodes (6BA6) with automatic and/or manual gain control. A low noise high slope RF pentode (6AR5) functions as the 1st Mixer with cathode injection from the Local Oscillator. The mixer operates with fixed cathode bias, no gain control being provided on this stage.

Permeability tuning is used in both the RF and Mixer Stages, a total of thirty-five variable inductances being required to cover the

complete tuning range. These inductances are selected by means of the wavechange Switch which also connects the required pre-set 'tuning' capacitors across them. It should be noted that some coils are used on more than one range, and in this case range selection is by means of the switched capacitors only. (See Detached Circuits Nos. 1, 2 and 3 which give the complete F and 1st Mixer range switching)

TABLE 2

Range	RF Coverage	Injection Frequency	IF Range
1	0.5 - 1.5 Mc/s	5 Mc/s	3.5 - 4.5 Mc/s ('B')
2	1.5 - 2.5 Mc/s	6 Mc/s	3.5 - 4.5 Mc/s ('B')
3	2.5 - 3.5 Mc/s	-	2.5 - 3.5 Mc/s ('A')
4	3.5 - 4.5 Mc/s	-	3.5 - 4.5 Mc/s ('B')
5	4.5 - 5.5 Mc/s	8 Mc/s	2.5 - 3.5 Mc/s ('A')
6	5.5 - 6.5 Mc/s	10 Mc/s	3.5 - 4.5 Mc/s ('B')
7	6.5 - 7.5 Mc/s	10 Mc/s	2.5 - 3.5 Mc/s ('A')
8	7.5 - 8.5 Mc/s	12 Mc/s	3.5 - 4.5 Mc/s ('B')
9	8.5 - 9.5 Mc/s	12 Mc/s	2.5 - 3.5 Mc/s ('A')
10	9.5 - 10.5 Mc/s	14 Mc/s	3.5 - 4.5 Mc/s ('B')
11	10.5 - 11.5 Mc/s	14 Mc/s	2.5 - 3.5 Mc/s ('A')
12	11.5 - 12.5 Mc/s	16 Mc/s	3.5 - 4.5 Mc/s ('B')
13	12.5 - 13.5 Mc/s	16 Mc/s	2.5 - 3.5 Mc/s ('A')
14	13.5 - 14.5 Mc/s	18 Mc/s	3.5 - 4.5 Mc/s ('B')
15	14.5 - 15.5 Mc/s	18 Mc/s	2.5 - 3.5 Mc/s ('A')
16	15.5 - 16.5 Mc/s	20 Mc/s	3.5 - 4.5 Mc/s ('B')
17	16.5 - 17.5 Mc/s	20 Mc/s	2.5 - 3.5 Mc/s ('A')
18	17.5 - 18.5 Mc/s	22 Mc/s	3.5 - 4.5 Mc/s ('B')
19	18.5 - 19.5 Mc/s	22 Mc/s	2.5 - 3.5 Mc/s ('A')
20	19.5 - 20.5 Mc/s	24 Mc/s	3.5 - 4.5 Mc/s ('B')
21	20.5 - 21.5 Mc/s	24 Mc/s	2.5 - 3.5 Mc/s ('A')
22	21.5 - 22.5 Mc/s	26 Mc/s	3.5 - 4.5 Mc/s ('B')
23	22.5 - 23.5 Mc/s	26 Mc/s	2.5 - 3.5 Mc/s ('A')
24	23.5 - 24.5 Mc/s	28 Mc/s	3.5 - 4.5 Mc/s ('B')
25	24.5 - 25.5 Mc/s	28 Mc/s	2.5 - 3.5 Mc/s ('A')
26	25.5 - 26.5 Mc/s	30 Mc/s	3.5 - 4.5 Mc/s ('B')
27	26.5 - 27.5 Mc/s	30 Mc/s	2.5 - 3.5 Mc/s ('A')
28	27.5 - 28.5 Mc/s	32 Mc/s	3.5 - 4.5 Mc/s ('B')
29	28.5 - 29.5 Mc/s	32 Mc/s	2.5 - 3.5 Mc/s ('A')
30	29.5 - 30.5 Mc/s	34 Mc/s	3.5 - 4.5 Mc/s ('B')

Two image filters are fitted in the aerial input circuit to assist in maintaining the image signals at a low level on the higher tuning ranges of the receiver. Filter 'A' (See Main Circuit Diagram Part 1) is of the low pass type and has a cut-off frequency of about 30.6 Mc/s. It remains in circuit on all ranges but only functions as an image filter at signal frequencies above 23.5 Mc/s. The filter is kept in circuit on all ranges to provide a constant aerial input impedance of approximately 75 ohms on all frequencies to which the receiver may be tuned. Filter 'E' (See Detached Circuit No. 1.) is brought into circuit on Ranges 14-17 to ensure an image response of better than -90dB

at all signal frequencies up to 15 Mc/s. The cut-off frequency of Filter 'E' is approximately 17.6 Mc/s and above 15 Mc/s the image rejection is better than -70dB.

The input circuit of the 1st RF Stage is provided with an 'Aerial Trimmer Control' (C166) which allows accurate adjustment of the first tuned circuit when using aerials of impedances differing appreciably from 75 ohms.

AGC bias is shunt fed to the two RF Stages via the feed resistors R1 and R6. Detuning effects are reduced to a minimum by returning the suppressor grids of the controlled stages direct to their cathodes.

Manual RF gain control is effected by taking the cathode bias resistors of the RF Stages to the junction of R10 and R11 via the common variable cathode resistor RV1. In normal operation, R11 is shorted out either by a wire strap across the de-sensitising terminals or a closed relay contact across the same points. This connects the RF Gain Control, RV1, direct to earth, giving normal bias to V1 and V2. The receiver is de-sensitised by open circuiting the terminals referred to above and under these conditions, the voltage developed across R11 is applied in series with the normal cathode voltage. This increases the bias applied to the RF Stages and so reduces their gain.

Low value grid stoppers, R2, R7 and R14 are fitted in the RF and Mixer Stages to ensure freedom from instability. The stages are well screened from one another for the same reason.

The 1st Local Oscillator Unit employs two sub-miniature 'high reliability' RF pentodes (6F732) as Crystal Oscillator and Buffer/Multiplier Stages. The whole unit is contained in a double screening box to prevent direct radiation and so permit receivers to be operated side by side without fear of interaction. A double screened coaxial output lead is used for the same reason, the inner screen being connected to the inner screening box and the outer screen to the outer box. The two boxes are insulated from one another, as are the screening conductors of the coaxial output lead. Earthing of the inner box occurs at the coaxial socket (SKT3) in the cathode of the 1st Mixer.

Both stages operate from a stabilised HT supply, and this and the LT supply are well filtered to prevent radiation from the wiring external to the screened boxes. In this way spurious responses are kept to a very low level (of the order of -120dB and greater)

The Crystal Oscillator always works on the fundamental crystal frequency, any necessary multiplication taking place in the following stage. A total of 10 crystals are used to cover the 28 ranges when the receiver functions with double conversion. Table 3 gives a full summary of the crystals used for the various ranges, indicating multiplication factors where applicable.

The required crystal is selected by the Wavechange Switch which also introduces the correct pre-tuned output circuit for the Buffer/Multiplier Stage. Sixteen separate output circuits are used and these are shown in Detached Circuit N. 5. Each output circuit is provided with a low impedance coupling coil which provides output to the cathode

of the 1st Mixer Stage. On Ranges 3 and 4 the 1st Oscillator Unit is disabled by the Wavechange Switch and in this way the 1st Mixer functions as an RF Amplifier from 2.5-4.5 Mc/s.

TABLE 3

Crystal Frequency	Multiplication Factor		
	X1	X2	X3
5 Mc/s	Range 1	-	-
6 Mc/s	Range 2	-	Ranges 14 & 15
8 Mc/s	Range 5	-	-
10 Mc/s	Ranges 6 & 7	Ranges 16 & 17	Ranges 26 & 27
11 Mc/s	-	Ranges 18 & 19	-
12 Mc/s	Ranges 8 & 9	Ranges 20 & 21	-
13 Mc/s	-	Ranges 22 & 23	-
14 Mc/s	Ranges 10 & 11	Ranges 24 & 25	-
16 Mc/s	Ranges 12 & 13	Ranges 28 & 29	-
17 Mc/s	-	Range 30	-

No crystals required on Ranges 3 & 4.

THE IF/AF SECTION

The output from the RF Section is applied to the tuned IF Stage (V4) via a low pass filter (Filter 'B') having a cut-off frequency of 4.9 Mc/s. This filter attenuates the higher frequency components in the mixer output so maintaining the spurious response at a very low level.

The tuned IF Stage (6BA6) feeds the 2nd Mixer which employs a 6AK5 with cathode injection from the 2nd Oscillator Unit. Both V4 and V5 input circuits are permeability tuned and ganged to the tuning of the RF and 1st Mixer Stages.

No manual gain control is applied to either stage since adequate adjustment of the overall IF gain is provided in the stages operating at the 'second IF'. AGC is applied to V4 via the feed resistor R22.

As in the RF Section, grid stoppers are fitted to both V4 and V5, and these, together with extensive screening, ensure stable operation.

The 2nd Local Oscillator Unit employs a 6U8 triode pentode as a combined electron coupled oscillator (V8B) and reactance control valve (V8A), together with the triode V9 (6C4) which functions as a cathode follower providing a low impedance output to the 2nd Mixer Stage V5.

The total coverage of the E.C.O. is 2.9-4.1 Mc/s inclusive of the 100 kc/s band edge overlaps, and whereas all other tuned stages employ permeability tuning, the 2nd Local Oscillator Unit uses a high quality variable capacitor which is ganged to the main tuning control.

To prevent harmonics of the oscillator reaching the Mixer Stage, two low pass filters (Filters 'C' and 'D') are incorporated in the 2nd Local Oscillator Unit. The unit itself is housed in a double screening box to prevent radiation of oscillator harmonics which would otherwise fall within the tuning range of the receiver. Radiation from wiring leaving the unit is avoided by filtering these leads at their point of exit. A coaxial output lead is used for the same reason.

V8 operates from the stabilised HT supply (108 volts), while the main HT line supplies the Buffer Stage V9.

The triode section of V8 is connected in parallel with the E.C.O. tuned circuit and allows the receiver to be remotely tuned as explained in the Section dealing with Installation.

The output from the 2nd Mixer is fed to a three stage amplifier operating at the 'second IF' of 500 kc/s. High slope vari-mu RF pentodes of the 6BA6 type are used in this amplifier which may be switched to give four degrees of IF selectivity, one of which involves the use of a dual crystal bandpass filter. A fifth position of the Selectivity Switch introduces an Audio Filter which supplements the selectivity of the crystal filter when receiving CW signals under conditions of severe adjacent channel interference.

Fig.4. shows in simplified form, the IF circuit coupling arrangements in each position of the Selectivity Switch. Switched tertiary windings are used to vary the coupling factor and the gain is maintained at a constant level by the switched taps on the circuit feeding the first stage. The crystal phasing capacitor is pre-set during alignment to produce a response having very steep sides with little or no evidence of the rejection notches due to the crystals. To prevent coupling to the crystals when the crystal filter is not in use, both crystals are shorted by the Selectivity Switch. The two crystals whose frequencies differ by 400 c/s are contained in a single B7G type holder.

AGC is applied to the first two stages, V10 and V11 via the feed resistors R56 and R61, while manual control of the overall IF gain is provided by RV2 which is in series with the cathode bias resistors of the same two stages. The third stage, V12, operates at fixed gain and feeds V13B, V14A, V14B and the miniature diode V21.

V13B ($\frac{1}{2}$ 6AL5) is the AGC Rectifier which controls the RF Amplifiers V1 and V2 and the IF Stages V4, V10 and V11 when AGC is in use. The AGC Switch, S4, provides a choice of two AGC time constants and AGC 'OFF'. A delay voltage of some 18-20 volts is applied to the cathode of V13B from the potential divider made up of R77 and R78.

Also controlled by the AGC line, is the DC Amplifier, V15A ($\frac{1}{2}$ 12AT7) which operates the carrier level meter when the AGC is in use. A pre-set control (RV3) is provided to permit accurate zeroing of the meter which is very useful in carrying out comparative checks on carrier levels.

V14A and B are fed in parallel from the secondary of T7, a 12AT7 double triode being used in this position. Both triodes function as

cathode followers, V14A providing a low impedance output for external use, while V14B feeds the CW/SSB Detector V16. This stage (V16) operates as a multiplicative mixer (product detector) and gives superior results to those obtained when using a conventional diode detector for CW and SSB reception. The injection frequency from the oscillator section (BFO) is variable over the range 500 kc/s plus or minus 6 kc/s by the BFO Control (C128).

The CW/SSB Detector is housed in a screening can to prevent radiation of oscillator harmonics which would otherwise cause interference throughout the tuning range of the receiver. The screen supply for V16 is obtained from a stabilised source and is applied during CW and SSB reception by one section of the Mode Switch (S5a).

Output from V16 is taken via the coupling capacitor C125 to the other section of the Mode Switch (S5b) either direct or via the Audio Filter dependent on the position of the Selectivity Switch S2.

The miniature diode V21, is used as detector for the reception of AM signals. Incorporated in the detector circuit is a series pulse limiter, V13A, which may be used to reduce impulse noise during AM reception. If not required, the limiter can be taken out of circuit by means of S3.

The detected signal output across R75 is fed to the grid of V15B ($\frac{1}{2}$ 12AT7) which provides additional audio amplification when receiving AM signals. This extra amplification compensates for the higher gain of the CW/SSB Detector and obviates the need for adjustment of the gain controls when moving the Mode Switch from one position to the other.

Provision is made in the grid circuit of V15B for connection of audio signals derived from an external source. Such signals may be introduced by means of a standard jack plug inserted into the socket JK1. Insertion of the plug automatically disconnects the detector output and prevents interference from normal signals. It should be noted that the Mode Switch must be in the AM position when the receiver is used in this way since V15B is not in circuit on CW and SSB.

S5b selects the required audio output from either V15B during AM reception, or V16 when receiving CW or SSB signals. Audio is fed via the switched bass filter to the AF Gain Control RV4 which functions on both internal and external audio signals. The audio voltage across RV4 is applied to the audio stage V17A ($\frac{1}{2}$ 12AU7) which operates in conjunction with the phase splitter (V17B) to provide a push-pull input to the AF Output Stage comprising V18 and V19. This stage, using a pair of 6AM5 pentodes, provides outputs for connection to high impedance telephones, loudspeaker and remote lines. Negative feedback is provided by R105 and R108 and a power output of up to 2 watts is available. It should be noted that inserting a pair of telephones disconnects the external loudspeaker and connects a loading resistor (R112) across the 2.5 ohm secondary winding of T9.

THE POWER SUPPLY SECTION

Apart from the use of miniature silicon rectifiers, this portion of the receiver is of fairly conventional design. Four of these rectifiers are used in a full wave circuit, the output of which is smoothed by the capacity input filter comprising C151, C152 and CH15.

V20 provides a 108 volt stabilised HT supply to V6, V7, V8, V16 (screen only) and the potential divider in the meter circuit. A separate HT supply is employed for V15B, V16 (anode) and V17 and is obtained from the junction of R113 and C150.

Three separate LT windings are provided on T10. All valve heaters with the exception of V13, are fed from the 6.3 volt 6 Amp winding (LT1) one side of which is earthed. The three dial lamps are also fed from this source via the variable resistor RV5 which provides a means of adjusting the brilliancy of the scale illumination.

V13 is fed from a separate winding (LT2) to prevent the introduction of hum in the noise limiter circuit. This winding is rated at 6.3 volts 0.5 Amps and its centre tap is returned to the junction of R115 and R116.

The remaining LT winding is connected to pins 3 and 6 of SKT7 and may be used as a heater supply for external units. Up to 3 Amps may be taken from the winding. (LT3). An associated HT supply is also available at SKT7 (pins 11 and 12), a maximum drain of 15 mA at 235 volts being permissible.

The receiver may be operated from external HT and LT supplies when an AC mains supply is not available. Full details are given later in the Section dealing with 'Installation'.

The AC mains input is switched in both live and neutral poles by the double pole switch S7. The live pole is fused at 1.5 Amp by the cartridge fuse FS1.

NOTE: Details of the Mains Transformer adjustments are given in the Section on 'Installation'.

MECHANICAL CONSTRUCTION

GENERAL

The Model 'S880' can be supplied as a standard rack mounting unit or as a table mounting unit. Either model may be converted to the other by removing certain parts of the existing cover and fitting plates etc. for the desired type of mounting. Conversion 'kits' are available to special order.

DIMENSIONS AND WEIGHT

Rack Mounted Version.

Width : 19 inches (48.3 cm) Depth : 20 1/2 inches (51.1 cm)
Height : 8 3/4 inches (22.2 cm) Weight : 75 pounds (34 kg)

Table Mounted Version.

Width : 19 1/2 inches (49.5 cm) Depth : 20 1/2 inches (51.1 cm)
Height : 9.7/16 inches (23.9 cm) Weight : 95 pounds (43 kg)

COVER

Rack and Table Mounted Models.

The main panel and chassis assembly together with the side plates, part of the top cover (actually the drive cover) and the combined rear and bottom cover are all common to both rack and table mounting models. Ventilation is provided by perforated areas in the rear cover and side plates, while access to the 1st Oscillator Unit is by means of a removable plate at the right hand side of the receiver (when viewed from the panel).

Rack Mounted Model.

In addition to the covers mentioned above, rack mounted models are fitted with a further top cover, which, together with the drive cover completely encloses the top of the receiver. Two small holes are provided in the drive cover for the 'Oddie' fasteners used to secure the lift-up lid fitted on the table mounted version. These holes are plugged with plastic inserts to prevent the ingress of dust etc. when the receiver is rack mounted.

Standard panel handles are fitted, but since the rack mounting model does not feature a panel escutcheon, small distance pieces are placed between the handles and the panel to ensure clearance of the controls should the receiver be placed 'face down' when carrying out maintenance.

Table Mounted Model.

A hinged lift-up lid is fitted in place of the fixed top cover

used on the rack mounting model. The hinges, which are of the lift-off type, are fitted to the top edge of the rear cover, the fixing holes being provided as a standard feature. Full instructions for removing the lid and details of the procedure for stripping either type of cabinet are given in the Section dealing with 'Maintenance'.

Close to the front edge of the lid are positioned the 'studs' of the two 'Oddie' fasteners which engage with clips located beneath holes in the drive cover - the plastic bungs fitted in the case of the rack mounted version are of course removed.

Specially shaped side covers are fitted in addition to the existing side plates. These are each fitted with three plastic mounting feet along the lower edge to prevent damage to the table surface and are provided with perforated areas to ensure adequate ventilation.

A panel escutcheon is fitted to increase the panel size slightly to match the styling of the cabinet and this escutcheon obviates the need for distance pieces when fitting the panel handles.

CHASSIS

Sub-chassis construction is employed throughout, all sub-chassis being built around a central 'RF frame' which is securely bolted to the rear of the two drive plates situated behind the front panel.

Six sub-chassis, together with two 'double screened' boxes go to make up the main assembly which is of extremely rigid construction when bolted together.

The six sub-chassis are as follows:-

- | | |
|----------------------|-----------------------------------|
| 1. 1st RF Amplifier. | 4. Tuned IF and 2nd Mixer Stages. |
| 2. 2nd RF Amplifier. | 5. IF/AF Chassis. |
| 3. 1st Mixer Stage. | 6. Power Unit Chassis. |

These, together with the two Oscillator Units, are inter-connected by a number of cable forms terminated in suitable plugs and sockets which permit units to be removed without resort to use of a soldering iron.

Both Oscillator Units and all sub-chassis except the Power Unit chassis are of brass, heavily silver plated and lacquered. The Power Unit chassis is of steel, suitably rustproofed and sprayed grey enamel.

PANEL

This is of $\frac{1}{8}$ " steel plate, hammer finished, with a cast escutcheon surrounding the dial aperture. A further escutcheon is fitted in the case of table mounted models, and this fits around and over the outer edge of the main panel slightly increasing its dimensions. A double anodised aluminium finger plate is fitted behind the receiver controls and labelled with their functions.

Chromium plated panel handles are fitted, and these, besides their

normal use in lifting the receiver, allow it to be placed 'face down' without damage to the controls.

TUNING DIAL AND DRIVE MECHANISM

The tuning dial occupies the top half of the front panel and has a single horizontal scale bearing calibration marks at 100 kc/s intervals. Direct frequency calibration is provided by three calibrated discs which are positioned behind apertures in the scale plate and rotated by the wavechange mechanism. Interpolation between the 100 kc/s points is achieved by means of a vernier scale located in the lower centre of the main scale.

The main tuning control operates a spring loaded split gear system which provides two main drive outlets together with a pulley drive for the scale pointer and a gear drive for the vernier scale.

One of the main drive outlets is coupled to the rotor of the tuning capacitor in the 2nd Oscillator Unit while the other drives a helical gear mechanism which raises and lowers the platform carrying the tuning cores for the RF, Mixer and Tuned IF Stages.

The gear ratios are such that it requires twenty-four revolutions of the main tuning control to move the pointer from end to end of its traverse, a total distance of some fourteen inches. At the same time, the vernier scale makes a total of twelve revolutions, each of which corresponds to a frequency change of 100 kc/s. The resulting tuning rate - 50 kc/s per revolution - is adequate for all types of reception.

INTER-UNIT WIRING

As mentioned earlier in this Section, all units are interconnected by means of cable forms terminated in suitable plugs and sockets to allow easy removal of individual units.

Five miniature six-way sockets located on the Power Unit chassis distribute the HT and LT supplies to the various sections of the receiver while three similar sockets are mounted on the rear of the front panel to provide connection to the panel controls.

To simplify the layout of the Main Circuit Diagram, none of the connectors referred to above have been shown. No confusion will result if it is borne in mind that the two potential dividers R10/R11 and R85/86 are located in the Power Unit.

THE HISTORY OF THE UNITED STATES

The history of the United States is a story of growth and change. From the first settlers to the present day, the nation has evolved through various stages of development. The early years were marked by exploration and settlement, followed by a period of rapid expansion and industrialization. The American Revolution and the Civil War were pivotal moments in the nation's history, shaping its identity and values.

The United States has a rich and diverse cultural heritage. The contributions of immigrants from various parts of the world have shaped the nation's identity. The American dream, the pursuit of happiness, and the principles of liberty and justice are central to the nation's history. The country has faced many challenges, but it has always emerged stronger and more united.

The history of the United States is a testament to the power of the human spirit. It is a story of resilience and innovation, of courage and sacrifice. The nation's history is a source of pride and inspiration for all Americans. It is a story that continues to unfold, and it is up to us to shape the future of this great country.

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INSTALLATION

MOUNTING

The Model 'S880' is supplied complete with all valves either as a table mounted unit or in a form suitable for rack mounting. When rack mounted, the receiver occupies $8\frac{1}{4}$ inches of height in a standard rack of 19 inch width. An area $19\frac{1}{2}$ " X $20\frac{1}{8}$ " is required for table mounting.

Four standard fixing slots are provided when the receiver is intended for use in a rack but no fixing is required in a table mounted installation.

When installing the receiver, due regard should be paid to positioning both for convenience in operation and ease of access to external connections at the rear.

When a number of receivers are mounted in a common rack (e.g. in a diversity installation), care should be taken to avoid obstructing the ventilation areas at the rear and in the sides of the cabinet.

EXTERNAL CONNECTIONS

Mains.

The three core PVC insulated lead should be terminated in a suitable three pin plug for connection to the local AC mains supply. The plug should be wired as follows:-

Red lead to live line.

Black lead to neutral line. Green lead to earth.

NOTE: Before connecting to the local AC mains supply, check that the mains transformer is adjusted for the appropriate voltage.
(see 'Mains Voltage Adjustment' later in this Section)

External Power Supplies.

Provision is made for the receiver to be powered from external HT and LT supplies when an AC mains supply is not available. The HT and LT voltages required are as follows and should be connected to a suitable 12 way female plug (Elcom) to mate with SKT7.

HT 235 volts at 145 mA. (DC)

LT 6.3 volts at 6.6 Amps. (DC)

These voltages may be obtained from any convenient source - a motor generator, vibrator pack, transistor convertor, or even direct from suitable accumulators. The HT supply is taken to the input side of the receiver filter circuit so that additional smoothing is available to supplement that provided in the external power supply.

NOTE: The negative sides of both HT and LT supplies are common connections and are earthed at SKT7.

The plug (PL5) should be wired as shown in Part 2 of the Main Circuit Diagram taking care not to omit the straps between pins 4 and 7 and 5 and 8. These links complete the heater supply to V13. Provision should be made to switch and fuse the external supplies at their source.

It should be borne in mind that the LT current drain of the Model 'S880' is quite high (6.6 Amps) and to avoid excessive voltage drop in the LT connections, these should be made with heavy gauge conductors.

When operating from AC mains supplies, a similar 12 way plug must be in place at SKT7 to complete the LT circuits from the transformer secondary windings to the valve heaters and dial lamps. The plug should be wired with straps between the following pins:-

1 and 4 2 and 5 7 and 10

If HT and LT supplies are required to power some small item of ancillary equipment, these may be taken from the same plug. (see PL6, Main Circuit Diagram - Part 2)

The voltages and currents available are as follows and under no circumstances should these values be exceeded.

HT		235 volts at 15 mA. (DC)
LT		6.3 volts at 3 Amps. (AC)

Aerial.

Connection is by means of a standard BNC coaxial plug terminating a 75 ohm coaxial line. A suitable plug is provided with the receiver. The input impedance is nominally 75 ohms unbalanced but other impedances may be used satisfactorily since provision is made for tuning the input circuit by means of the Aerial Trimmer, C166.

Earth.

A short direct lead of heavy gauge wire should be taken from this terminal to a suitable earthing point.

NOTE: When the receiver is supplied from a source which includes a circuit breaker (earth trip) no connection should be made to the earth terminal.

Loudspeaker.

An external loudspeaker may be connected to the two quick-release terminals marked 2.5 ohms. Any 2.5-3 ohms loudspeaker may be used, but the EDDYSTONE Cat. No. 688E is recommended as it matches the receiver both electrically and in finish.

Telephones.

If loudspeaker reception is not required, telephones may be plugged into the jack at the left hand side of the front panel. Although the output impedance is nominally 2000 ohms, lower telephone impedances may be used satisfactorily.

Insertion of the telephone plug disconnects the loudspeaker and connects a loading resistor (R112) across the 2.5 ohm secondary winding of T9.

Line Output.

Connection is made to the quick-release terminals marked 600 ohms. If a balanced output is required, the centre terminal (CT) should be connected to earth.

IF Output.

Connection should be made by means of a standard BNC coaxial plug terminating a 75 ohm coaxial line. The output available is an unrectified 500 kc/s IF signal and may be connected to a suitable FSK adaptor or other ancillary equipment.

AF Input.

When required, the receiver may be used as an AF Amplifier. Connection should be made to JK1 using a standard GPO jack plug, the sleeve of which is the earth connection. Insertion of the plug automatically disconnects the audio output from the AM Detector so preventing interference from received signals.

An output of up to 2 watts is available and the Bass Switch and AF Gain function normally when the receiver is used in this way.

NOTE: The Mode Switch must be in the AM position when external audio signals are used.

AGC Terminal.

When two or more Model 'S880' receivers are used under diversity conditions, their AGC Terminals should be joined together. In this way the operative AGC voltage will be that due to the receiver with the greatest input and the rising noise of the other receiver(s) will be suppressed.

Because of the high stability of the Model 'S880', provision of a common oscillator system as used in many diversity installations is entirely unnecessary.

When setting up a number of receivers for diversity working, the built-in carrier level meter should be used to ensure correct tuning.

Oscillator Remote Control.

Fine tuning of the receiver may be carried out from a distant listening point if use is made of the Reactance Control Valve (V8A).

Under normal conditions, the bias on this stage is fixed by its cathode resistor R42, the terminals marked 'G' and 'K' being strapped to terminal 'E' (earth). Removing the strap across terminals 'E' and 'K' will cause the bias on V8A to increase due to the voltage drop across the now unshorted resistor R39. A 1000 ohm variable resistor connected across R39 (i.e. between 'E' and 'K') will provide a means of altering

the bias on V8A and therefore the frequency of the VFO (V8B) so tuning the receiver independently of the main tuning control.

It will be realised that this simple method entails 'off-tuning' the receiver slightly so that the correct frequency obtains when the variable resistor is set to 500 ohms. If this adjustment is not carried out, tuning will be possible in one direction only.

A more elaborate method is to remove both shorting straps and connect terminal 'G' to the slider of a potentiometer across the output of a low voltage power supply. The negative side of the power supply should be connected to terminal 'E' so that the bias on the control grid of V8A may be set positive by an amount equal to the increase in cathode bias due to removal of the strap across R39.

When the latter method is employed, 'off-tuning' will not be necessary since complete control is available by means of the potentiometer.

NOTE: When remote tuning is not required, terminals 'G' and 'K' must be strapped to terminal 'E' otherwise the dial calibration will be upset.

External Relay Terminals.

When de-sensitising facilities are required, an external relay contact may be connected to the two quick-release terminals marked 'D' and 'E'. This contact should be arranged to close when the receiver is required to function normally and open to de-sensitise the receiver when an associated transmitter is in operation.

If de-sensitising is not required, the two terminals must be connected together by means of a wire strap.

MAINS VOLTAGE ADJUSTMENT

As despatched, the mains transformer tapplings are set for 240V operation. When operation is to be from other mains voltages, the tapplings should be set as shown in the table below.

TABLE 4.

Voltage	Strap	Input to	Voltage	Strap	Input to
100	C & D E & H	C & H	200	D & E	C & H
110	C & D F & G	C & G	210	D & F	C & H
115	A & B E & H	B & H	220	D & F	C & G
125	A & B F & G	A & G	230	A & E	B & H
			240	A & E	B & G
			250	A & F	B & G

OPERATION

CONTROL FUNCTIONS

Tuning and wavechange.

These two controls, operated in conjunction with one another, determine the frequency to which the receiver is tuned. Dial calibration is presented in such a manner that the only figures visible are those applicable to the range in use. This is achieved by means of three calibrated discs rotated by the wavechange mechanism and appearing behind suitably positioned apertures along the main tuning scale.

Rotation of the tuning control causes a pointer to traverse this scale which has a length of some 14 inches and bears calibration marks at 100 kc/s intervals. Interpolation between these points is provided by a vernier scale which is graduated into 100 divisions each representing 1 kc/s. This scale is conveniently located above and between the Tuning and Wavechange controls.

In point of fact, the vernier carries two scales, one printed in red, the other black. The red scale is calibrated in the reverse direction to the black scale and is intended for use when operating on Ranges 3 and 4 which employ 'reverse' tuning. (see 'Circuit Description. Likewise, the main scale calibration appears in red on these two ranges and is a reminder to the user that the scale must be read in reverse.

Aerial Trimmer.

Provides a means of accurately resonating the aerial input circuit. In operation, this control should always be peaked - either on background hiss or a received signal - to give maximum audio output.

Gain Controls.

Three gain controls are provided, these being as follows:-

- RF Gain (RV1) Controls V1 and V2.
- IF Gain (RV2) Controls V10 and V11.
- AF Gain (RV4) Controls input to Audio Section with either internal or external AF signals.

The RF Gain should be well advanced during all types of reception since the best signal-to-noise ratio will result under this condition of operation. When receiving CW signals, however, it may be necessary to reduce the RF Gain to supplement the control range of the IF Gain. This latter control will, at normal signal levels, give an adequate range of adjustment of pre-detector gain.

When searching for signals, the RF Gain should be fully advanced and the IF Gain set to give a barely audible noise level.

The AF Gain will prove most useful during AM reception when the RF and IF Gains are well advanced to secure the best possible AGC action.

Selectivity Switch.

Five degrees of selectivity are provided, ranging from 14 kc/s at 6dB down in the 'BROAD' position to 400 c/s at 6dB down in the 'CRYSTAL' position. With the Audio Filter in circuit the overall bandwidth becomes 100 c/s at 6dB down and this position is of immense value when receiving CW signals under conditions of severe adjacent channel interference. The 'BROAD' position will provide excellent quality from broadcast stations when the receiver is used as a terminal for recording or re-transmission purposes.

For communications work, increasing the selectivity will improve the signal-to-noise ratio without making tuning unduly critical.

BFO Adjustment.

Varies the 'pitch' of the audio beat note when receiving CW signals. The control may be set so that the injected frequency from the oscillator lies on either side of the IF passband so providing a means of 'single signal' CW reception with attenuation of either the HF or LF adjacent channel as required.

In SSB reception the BFO should be set to correspond with the sideband in use, and, once set should require no further adjustment.

Bass Switch.

Provides facilities for reducing the bass response of the Audio Section when receiving AM signals suffering from low frequency heterodyne interference.

When external audio signals are fed to the receiver, the switch functions as a tone control in the normal way.

Mode Switch.

This control selects audio output from the appropriate Detector for either AM or CW and SSB reception. The screen voltage is removed from V16 during AM reception.

AGC Switch.

Provides a choice of either automatic and/or manual gain control of the pre-detector stages.

Two positions of AGC are provided, namely 'AGC FAST' and 'AGC SLOW'. In the 'FAST' position, the time constant of the AGC circuit is adjusted to suit the reception of rapidly fading telephony signals or high speed automatic telegraphy. For slower speed telegraphy a longer time constant is required and this is provided in the 'SLOW' position.

Noise Limiter Switch.

This control is only operative during the reception of AM signals. Placing the switch to the 'ON' position introduces a series pulse limiter into the Detector circuit and this is effective in reducing impulse noises which may be experienced during AM reception.

Mains Switch.

Makes or breaks both live and neutral poles of the AC supply to the mains transformer T10.

The Mains Switch performs no function when the receiver is used with external power supplies.

Meter Zero Adjustment.

Permits adjustment of the meter needle to zero before comparative checks of carrier level are made.

Dial Lamp Brilliancy.

A pre-set control located at the rear of the receiver. Allows the dial illumination to be set to suit the conditions under which the receiver is used.

TUNING INSTRUCTIONS

Preliminary.

Check that the AC mains supply or external HT and LT supplies are available. Check all external connections and ascertain that a suitable aerial is in use. Either connect a loudspeaker, or if speaker reception is not required, plug a pair of high impedance telephones into the socket on the front panel.

Next place the Mains Switch to 'ON'. (In the case of operation from external supplies, the Mains Switch may be left 'OFF' but the external supplies should be switched on at their source) An indicator that the receiver is operative is given by the illumination of the tuning dial. The brilliancy of this lighting can be set as required by means of the control at the rear of the receiver.

While the receiver is warming up, the following adjustments may be carried out. Firstly, select the appropriate range and tune to the required frequency.

NOTE: When using Ranges 3 and 4, scale calibration appears in red and this indicates that the scale (and the vernier) should be read in the reverse direction to the other ranges.

If AGC is to be used, place the AGC Switch to 'FAST' or 'SLOW' (as appropriate to the type of reception) and, when background noise becomes apparent, adjust the gain controls to provide a suitable output. The Aerial Trimmer may now be peaked and the required degree of selectivity obtained by adjustment of S2.

AM Reception.

Place the Mode Switch to AM and, having obtained the desired signal, make any re-adjustments as required. If impulse noise is troublesome the Noise Limiter Switch may be placed in the 'ON' position. The Bass Switch should be set to provide the desired audio response.

CW Reception.

With the Mode Switch at CW/SSB and the BFO offset from zero, tune in the required signal and by alternate adjustment of the BFO and Tuning Control (and selectivity if necessary) obtain the best conditions of reception.

NOTE: The Noise Limiter is inoperative in the CW/SSB position of the Mode Switch.

SSB Reception.

With the AGC 'ON' and the Mode Switch to AM, tune the receiver for maximum deflection of the carrier level indicator. Switch to CW/SSB and with the AGC 'OFF', adjust the BFO for clear intelligible speech. The Main Tuning Control should not be touched and the Selectivity Switch should be placed in the 'NARROW' position.

ADJUSTMENT OF THE METER ZERO

To accurately adjust the meter needle to zero before carrying out comparative checks on carrier levels, first remove the aerial and connect a 75 ohm carbon resistor across the aerial socket.

With the RF and IF Gain Controls set to maximum and with the AGC at either 'ON' position, adjust the Meter Zero Control (using a screwdriver) so that the meter needle is coincident with the '0' mark on the meter scale.

The meter scale is calibrated in 6dB steps from 0-9, while above 9, calibration is directly in decibels.

MAINTENANCE

GENERAL

The Model 'S880' is intended for continuous operation in all areas regardless of climatic conditions and should require very little in the way of maintenance over long periods of use.

As with any piece of electronic equipment, periodical dust removal should be carried out, preferably with a compressed air blower.

All switches used in the receiver are of the self-cleaning type and should therefore require no attention. All moving parts are lubricated with a permanent lubricant (molybdenum disulphide) so that regular lubrication is unnecessary. If, however, after long periods of use, lubrication is thought necessary, any light mineral oil (suitable for the temperature conditions under which the receiver is operated) may be used.

External connections, especially telephone leads should be checked from time to time to ensure complete serviceability.

DIAL LAMP REPLACEMENT

Faulty dial lamps may be replaced quickly and without difficulty by removing four fixing screws and lifting up the drive cover immediately behind the top edge of the front panel. In the case of rack mounted receivers, the front edge of the cover should be tilted upwards to clear the main top cover of the cabinet. The three lamp holders are fitted to the underside of the drive cover which may be removed completely by taking out the miniature plug at the right hand side.

To change a bulb, merely ease back one of the spring contacts, slip out the faulty bulb and fit the replacement.

6 volt 3 watt 'Festoon' bulbs should be used as spares.

FUSE REPLACEMENT

The fuse (FS1) fitted in the Model 'S880' lies in the live mains input lead so that failure will result in complete loss of power to the receiver.

A faulty fuse may be changed by unscrewing the fuse holder located at the rear of the receiver (L.H.S.). A 1.5 Amp cartridge type fuse should be used for replacement and two of these are provided in clips located on the platform cover.

If the replacement fuse blows immediately the receiver is switched on, or fuses burn out regularly over short periods of operation, checks should be made to ascertain the cause.

VALVE REPLACEMENT

Of the valves visible on removing the top cover or lifting the lid (as appropriate), all except the two output valves may be removed without using the valve extraction tool provided. Removal of V18 and V19 can be accomplished quite simply by use of the extraction tool.

Replacement of the valves in the Oscillator Units is a little more involved but should present no difficulty if the instructions given below are carefully followed.

Replacement of V6 and V7. (1st Oscillator Unit)

First, remove the alignment plate at the right hand side of the receiver to expose the outer cover of the 1st Oscillator Unit.

In the case of table mounted models it is necessary to remove the shaped side cover to gain access to the alignment plate. The procedure is quite simple - merely slacken off the three 2BA screws at the rear of the cover and the two $\frac{1}{4}$ " BSF 'Allen' types situated behind the panel handle. The cover is provided with slots which locate with these fixing points and allow it to be lifted clear without removing the screws completely. The same procedure should be adopted when it is necessary to remove the left hand cover during IF alignment.

Next, take out the seven 6BA screws and remove the outer cover by

sliding out from under the flange at the lower edge. This will reveal the inner cover which may be removed in the same way.

Once the inner cover is removed, the turret lugs to which the valve connections are soldered will be clearly visible. V6 is above V7 when the crystals lie to the left of the valve positions.

A faulty valve may easily be removed by unsoldering the connections to the turret lugs and withdrawing the valve from its clip.

When fitting replacement valves of this type (EF732), soldered connections must be at least 5 mm from the glass seal and should be made using a thermal shunt. Bends in the lead out wires must be at least 1.5 mm from the glass seals. Orientation of the valve lead out wires should be checked before removing the faulty valve.

Having replaced the faulty valve, check the receiver for normal operation before replacing the unit covers, alignment plate etc.

Replacement of V8 and V9. (2nd Oscillator Unit)

Access to V8 and V9 is from the top of the 2nd Oscillator Unit. First remove the four screws securing the outer cover. In lifting this cover away from the unit some resistance will be felt; this is due to the spring earthing strip along the inside edges.

Two inner covers will now be visible, one being hinged at the centre where the two covers meet. This hinged cover can only be lifted by removing the two screws securing the strip carrying the feed-through capacitors and taking off the 'push-fit' front cover. V8 is located beneath the front cover and V9 beneath the hinged cover at the rear. When lifting the rear cover, remove PL4 from SKT4 and feed the coaxial output lead through the hole in the left hand side of the outer box and the hole in the inner cover so that the cable receives no strain when the cover is lifted.

Both V8 and V9 are secured by clips and these should be carefully replaced whenever a valve is changed.

In replacing the covers, do not omit to replace the two screws holding the feed-through strip and ensure that the edges of the outer cover and front inner cover which carry no earthing strip are towards the rear of the receiver.

NOTE: Care should be taken when working on either of the Oscillator Units not to drop screws or other metallic objects into the gaps between the inner and outer boxes. Such items of hardware if left in place would most certainly short circuit the inner and outer boxes and impair their screening properties.

CRYSTAL REPLACEMENT

XL1 and XL2.

These two crystals which are used in the 500 kc/s IF crystal filter, are located in a holder mounted on the top of the large IF transformer T2. Both crystals are contained in a single B7G type envelope and replacement is simple and straightforward.

XL3 - XL12. (See Corrigendum at rear of manual.)

These ten crystals are located in the 1st Oscillator Unit. To remove and replace, it is necessary to open up the 1st Oscillator Unit as described above - see 'Replacement of V6 and V7'.

The crystals are positioned in two rows of five crystals to the left of V6 and V7. Correct positions for the crystals are as follows:-

Top row, reading from left to right (all frequencies in Mc/s)

17 - 13 - 16 - 14 - 12

Bottom row.

5 - 6 - 8 - 10 - 11

It is most unlikely that a crystal would ever need changing, but should it prove necessary, reference should be made to the Section dealing with 'Re-alignment'.

REMOVAL OF LID - TABLE MOUNTING MODEL ONLY

It may prove convenient to remove the lift-up lid completely when carrying out maintenance on the table mounted version.

Removal is accomplished by first taking out the retaining stop from the lid stay and then removing the two screws which secure the left hand hinge to the top edge of the rear cover. The lid can then be removed by disengaging the right hand hinge and sliding the stay clear of its slot.

The procedure for further stripping of the cabinet will be obvious upon inspection, no involved operations being called for. This is also true of the rack mounted model since the greater part of the cabinet is common to both models.

FAULT LOCATION

Faults falling in the categories 'loss of output', 'low sensitivity and in some cases 'faults of an intermittent nature' may be localised by application of straightforward signal tracing techniques. The 'sectional construction of the Model 'S88C' makes it an ideal subject for this type of fault location.

For example, the Audio Section may be checked by injecting an AF signal at JKL. An input of 8 mV (400 c/s) should produce a 50 mW output with the AF Gain and Bass Switch at maximum. The Mode Switch must be set to AM for this simple test which will reveal immediately whether the Audio Section is functioning or not.

A fault in the AM Detector circuit is an obvious conclusion if the set appears 'dead' when it is known that the Audio Section is functioning normally and signals are available at the IF Output Socket SKT6, while the Mode Switch is set to AM.

The 2nd Mixer Stage (V5) and the 500 kc/s IF Stages (V10, 11 and 12) are easily checked by injecting a modulated 500 kc/s signal at SKT4.

Likewise the operation of the tuned IF Section may be checked with a suitable signal introduced at SKT3. (see 'Re-alignment')

If an output is obtained with a 500 kc/s signal introduced at SKT4 but no output is available with a suitable signal injected at SKT3, the fault may be in the 2nd Oscillator Unit. This may be verified by removing PL4 and, with the receiver aerial connected, introducing at SKT4 a 'substitute' oscillator signal from a signal generator. Some 200 mV will be required and the generator output impedance should be low (75 ohms). Tune the receiver to any frequency and swing the generator tuning over the 3.0 - 4.0 Mc/s range. If normal reception is possible when the generator is tuned in step with the receiver tuning, it is a clear indication that the fault lies in the 2nd Oscillator Unit.

NOTE: Remember that the 2nd Oscillator tunes in the reverse direction to the RF tuning as explained in the Section dealing with 'Circuit Description'.

A similar test may be carried out at SKT3 if the 1st Oscillator Unit is suspected, but will require a greater level of injection voltage (upwards of 400 mV).

Once a fault has been localised to a certain section of the receiver, normal servicing techniques, voltage checks, substitution of valves, checking components etc., will quickly reveal the faulty stage.

RE-ALIGNMENT

General.

Although more complex than the average communications receiver, complete re-alignment of the 'S880' is simplified by virtue of the fact that the 1st Oscillator requires no adjustment and the 2nd Oscillator, once set to its fixed coverage (3.0 - 4.0 Mc/s), ensures accurate calibration on all ranges. The user should not be deterred by the number of stages involved in complete re-alignment since it is most unlikely that such a task would ever be necessary.

It is advisable, however, that partial re-alignment be carried out should it be necessary to change a faulty valve or component. Such adjustment should be restricted to the circuits associated with the stage or stages involved: for example, replacement of V8 may call for slight adjustment of C51 and L11, but no other adjustment need be made.

Provided suitable test equipment is available, re-alignment of any portion of the receiver may be carried out speedily and efficiently by reference to the instructions given in this Section.

Test Equipment.

The Table on the following page gives details of the test equipment and associated equipment required to satisfactorily re-align the various stages of the Model 'S880'. Three trimming tools are provided with the receiver, and these are located on the top of the platform cover in the centre of the chassis.

TABLE 5.

Section	Items required
500 kc/s IF Amplifiers	1. Sweep Generator capable of providing a 'centre sweep frequency' of 500 kc/s, with suitable 'scope. 2. Modulated Signal Generator capable of tuning to 500 kc/s. NOTE: Both the above to have coaxial output leads terminated in Belling Lee Type L.734/P coaxial plugs. 3. Output Meter matched to either 2.5 or 600 ohms. 4. Trimming Tools:- Neosid Type N.S.1. and screw-driver types with broad and narrow blades.
Oscillator Units	1. Frequency Meter or Crystal Calibrator covering the range 3.0 - 34.0 Mc/s - accuracy 0.003%, provided with output lead terminated in Belling Lee Free Socket Type L.734/J (or plug Type L.734/P with coaxial line coupling Type L.616.) 2. Valve Voltmeter, 1.5v. f.s.d. 3. Trimming Tools:- Broad and narrow screwdriver and Phillips concentric trimmer type.
Tuned IF and RF Sections	1. Modulated Signal Generator covering the range 500 kc/s - 30.5 Mc/s. Output lead terminated with an adaptor to suit both Belling Lee Type L.604/S and standard BNC coaxial sockets. 2. Output Meter matched to either 2.5 or 600 ohms. 3. Trimming Tool:- Narrow bladed screwdriver type.

Re-alignment of the 500 kc/s IF Amplifiers.

Switch on the receiver, sweep generator and oscilloscope and, while warming up, set the receiver controls as follows:-

Selectivity Switch	'Crystal'	AGC Switch	'Off'
Mode Switch	'AM'	NL Switch	'Off'
IF Gain	'Maximum'	Bass Switch	'Maximum'

Remove PL4, connect the output lead from the sweep generator to SKT4 and a screened lead from the Oscilloscope 'Y' plate amplifier between the Noise Limiter Switch and chassis, i.e. across the lower part of the AM Detector load. The AF Gain should be reduced and telephones plugged in

~~to effectively mute the Audio Section of the receiver.~~

Having set the generator to sweep the IF passband, adjust all IF transformer cores commencing at T7 secondary and working back to the primary winding of T1, trimming for greatest amplitude and symmetrical response. Two points of resonance will be obtained with each core; the correct one to use is that occurring when the core is furthest from the opposite coil. Side responses due to the crystals may be balanced by means of the phasing capacitor C80, the rejection notches being well down on the skirts and scarcely discernible when the adjustment is correctly made.

NOTE: Refer to Fig.5. for identification of primary and secondary cores, both of which are adjusted from the top using a Neosid trimming tool Type N.S.1. The lower core in each case is, of course opposite to the one indicated. The cores used have an hexagonal bore which runs completely through the core and allows one end of the trimming tool (provided with a shank of reduced diameter) to be passed through the top core for adjustment of the lower winding. Adjustment is quite straightforward and the cores are self-locking. The crystal filter output coil (T2) is adjusted through the LOWER, and the phasing capacitor (C80) through the UPPER of the two holes provided in the receiver side plate. (In the case of table mounted receivers, the shaped side cover (L.H.S.) must be removed to gain access to these adjustments and instructions for its removal are given elsewhere in this Section. (see 'Replacement of V6 and V7')

Having aligned the amplifier in the 'Crystal' position, check that the response is symmetrical in the other positions of the Selectivity Switch. It may be found necessary to adjust T2 slightly in the 'Broad' position and this can be done quite simply without upsetting the response in the other positions of the switch.

A sensitivity check may now be carried out with S2 at 'Narrow' using a standard signal generator. With 30% modulation at 400 c/s and with the signal introduced at SKT4, an input of approximately 1 uV should give an output of 50 mW. If the sensitivity appears low, stage by stage checks will reveal the faulty stage. The following figures are indicative of the sensitivities to be expected, and in each case the signal is introduced via the grid capacitor of the stage being checked (C83, 91 and 99 respectively).

V10	. .	2 uV for 50 mW output.
V11	. .	30 uV for 50 mW output.
V12	. .	5 mV for 50 mW output.

If a sweep generator is not available, alignment may be carried out using a standard signal generator and output meter but great care should be exercised in adjusting the phasing capacitor C80.

Re-alignment of the BFO.

First set the BFO Tuning Control (C128) to '0' on its scale and check that the mark on the control shaft (adjacent to the BFO Unit)

is positioned vertically with respect to the shaft indicating that the capacitor is at 'half-capacity'.

Inject an unmodulated signal in the centre of the IF passband and, with the Mode Switch to CW/SSB adjust L25 (see Fig. 5.) for zero beat using a large insulated screwdriver type trimming tool.

Re-alignment of the 1st Oscillator Unit.

It is most unlikely that adjustment of this unit will ever be necessary but details are given here for the sake of completeness.

Place the receiver on end, right hand side uppermost and remove the 1st Oscillator alignment plate. (In table mounted receivers it will be necessary to remove the shaped side cover to expose the alignment plate - see 'Replacement of V6 and V7').

Next, remove the outer and inner covers of the 1st Oscillator Unit (accessible when the alignment plate is removed).

Remove PL3 from SKT3 and connect PL3 to a suitable frequency standard. Switch on the receiver and frequency standard and allow adequate time for both to reach operating temperature. Select the appropriate receiver range and, with the frequency standard set to the frequency indicated in the Table below, adjust the correct trimmer to nullify any inaccuracy in the crystal frequency. All trimmers are mount adjacent to their appropriate crystal.

TABLE 6.

Range	Standard	Trimmer	Range	Standard	Trimmer
1	5 Mc/s	C314 ✓	10	14 Mc/s	C309 ✓
2	6 Mc/s	C313 ✓	12	16 Mc/s	C308 ✓
5	8 Mc/s	C312 ✓	18	22 Mc/s	C307 ✗
6	10 Mc/s	C311 ✓	22	26 Mc/s	C306 ✓
8	12 Mc/s	C310 ✓	30	34 Mc/s	C305

Having 'zeroed' all the crystals, disconnect the frequency standard and connect PL3 to a valve voltmeter of approx 1.5 volts F.S.D..

Select the ranges indicated in Table 7. and adjust the appropriate inductances for maximum reading in the valve voltmeter.

The unit may now be re-connected, no further adjustment being required.

Re-alignment of the 2nd Oscillator Unit.

First remove PL4 from SKT4 and connect PL4 to a suitable frequency standard. The reactance control terminals ('G', 'E' and 'K') at the rear of the receiver must be connected together by means of wire straps before alignment is commenced.

TABLE 7.

Range	Inductance	Range	Inductance
1	L70	16	L78
2	L71	18	L79
5	L72 — <i>BRIDGE</i>	20	L80
6	L73	22	L81
8	L74	24	L82
10	L75	26	L83
12	L76	28	L84
14	L77 —	30	L85

NOTE: The 'body' of PL4 must be earthed to the chassis of the receiver to complete the 'earthy' side of the HT and LT supplies to the Oscillator Unit. (Earthing normally takes place at SKT4)

Remove the top outer cover of the 2nd Oscillator Unit (immediately to the right of the tuning platform) to reveal the two inner covers, the front one of which is provided with two holes for adjustment of L11 and C51.

Switch on the receiver and frequency standard and allow adequate time for both to reach operating temperature.

Set the frequency standard to 3.0 Mc/s and, though it is immaterial which range is selected, it is convenient to place the receiver Wavechange Switch at Range 1 so that reference may be made to the dial calibration. Adjust the main tuning control so that the tuning pointer coincides with the calibration mark at 1.5 Mc/s and monitor the output from the frequency standard to ascertain what error (if any) exists.

Now alter the frequency standard to 4.0 Mc/s, set the receiver tuning pointer coincident with the 0.5 Mc/s calibration mark and check the accuracy at this point.

NOTE: The 2nd Oscillator tunes in the reverse direction to the RF tuning as explained in the Section headed 'Circuit Description'.

If any error exists, it may be corrected by adopting standard tracking technique in adjusting C51 (Phillips trimming tool) at the 4 Mc/s point and L11 (Insulated screwdriver type trimming tool) at the LF end of the Oscillator range (3 Mc/s).

Once the 'end' frequencies are correct, a check should be made at each of the 100 kc/s points along the tuning scale, remembering that the Oscillator tuning and scale calibration are reversed. Errors at these points are most unlikely since the tuning capacitor used is of the straight-line-frequency type and once the 'end' frequencies have been established no further adjustment should be necessary.

Re-alignment of the 'Tuned' IF Section.

Switch on the receiver and signal generator and allow adequate

time for both to reach operating temperature. Remove PL3 from SKT3 and connect the output lead from the generator to SKT3.

With the receiver controls set as when checking the sensitivity of the 500 kc/s stages, and with an output meter connected to either the 2.5 or 600 ohm terminals, select Range 3 and tune the receiver and signal generator to 3.0 Mc/s (generator modulated 30% at 400 c/s). Using a small screwdriver type trimming tool adjust the 2.5-3.5 Mc/s 'Tuned' IF and 2nd Mixer cores for maximum output. (See Fig. 5 for location of these trimming adjustments which are situated on the tuning platform.)

Now alter the generator tuning to 4.0 Mc/s and, without touching the receiver tuning, set the receiver Wavechange Switch to Range 4. This automatically tunes the receiver to 4.0 Mc/s and the 3.5-4.5 Mc/s cores should be peaked for maximum output.

A sensitivity check may now be carried out and should result in an output of 50 mW for an input of approximately 5 uV (signal introduced at SKT3). Checks should be made at both alignment frequencies.

NOTE: The lower sensitivity at this point compared with that at SKT4 is due to the fact that V5 is now functioning as a mixer, whereas previously when checking the 500 kc/s stages, V5 operated as an amplifier. When used as a mixer, V5 is operated with very low oscillator injection (in the interests of reduced radiation) and under conditions of minimum noise factor.

Re-alignment of the RF Section. (V1, 2 and 3)

Complete re-alignment of the RF Section will only be required if it has been necessary to remove the tuning platform - a most unlikely operation.

Fig. 5. shows the location of all trimming capacitors and cores applicable to RF alignment, and these are labelled for convenience, not with the circuit reference number, but with the range to which they apply. Also shown is a grid reference system which simplifies location of the correct trimmer on the 2nd RF and 1st Mixer sub-chassis. On Fig. 5. locate the desired trimmer - say 2nd RF, Range 21 - and obtain the reference 'A-3'. This same reference appears on the receiver sub-chassis and enables the correct trimmer to be located without error. On the tuning platform the range is indicated directly, no reference system being required.

The instructions given below are for complete re-alignment. No adjustments are necessary when a valve is replaced but partial re-alignment must be carried out should it be necessary to change a component associated with the tuned circuits. Such re-alignment only calls for adjustment of the circuit concerned and no further trimming should be attempted.

In carrying out complete re-alignment, first switch on the receiver and generator and while these reach operating temperature, connect a suitable output meter and set the receiver controls as follows:-

Selectivity Switch	'Narrow'	AGC Switch	'Off'
Mode Switch	'AM'	NL Switch	'Off'
RF, IF and AF Gains	'Maximum'	Bass Switch	'Maximum'

Connect the signal generator output lead to the receiver aerial socket (.BNC plug) and set the tuning control so that the pointer lies on the 'Megacycle point' at the centre of the scale. Check that the vernier scale reads zero. Once set, the tuning control should not be touched throughout the whole alignment.

Set the generator modulation depth at 30% (400 c/s), select the receiver ranges and generator frequencies indicated in the Table below and adjust the appropriate trimmers or cores for maximum output reading.

TABLE 8.

Range	Sig. Gen.	1st RF Stage		2nd RF Stage		1st Mixer Stage	
		Trimmer	Core	Trimmer	Core	Trimmer	Core
1	1 Mc/s	NIL	L41	NIL	L53	NIL	L65*
2	2 Mc/s	NIL	L40	NIL	L52	NIL	L64
3	3 Mc/s	NIL	L39	NIL	L51	NIL	L63
4	4 Mc/s	NIL	L38	NIL	L50	NIL	L62
5	5 Mc/s	NIL	L37	NIL	L49	NIL	L61
6	6 Mc/s	NIL	L36	NIL	L48	NIL	L60
7	7 Mc/s	NIL	L35	NIL	L47	NIL	L59
8	8 Mc/s	NIL	L34	NIL	L46	NIL	L58
9	9 Mc/s	NIL	L33**	C223(A6)	L45**	C278(E6)	L57**
10	10 Mc/s	NIL		C222(B6)		C277(F6)	
11	11 Mc/s	NIL	L32**	C221(C6)	L44**	C276(G6)	L56**
12	12 Mc/s	NIL		C220(D6)		C275(H6)	
13	13 Mc/s	NIL		C219(A5)		C274(E5)	
14	14 Mc/s	NIL	L31**	C218(B5)	L43**	C273(F5)	L55**
15	15 Mc/s	NIL		C217(C5)		C272(G5)	
16	16 Mc/s	NIL		C216(D5)		C271(H5)	
17	17 Mc/s	NIL		C215(A4)		C270(E4)	
18	18 Mc/s	NIL	L30**	C214(B4)	L42**	C269(F4)	L54**
19	19 Mc/s	NIL		C213(C4)		C268(G4)	
20	20 Mc/s	NIL		C212(D4)		C267(H4)	
21	21 Mc/s	NIL		C211(A3)		C266(E3)	
22	22 Mc/s	NIL		C210(B3)		C265(F3)	
23	23 Mc/s	NIL		C209(C3)		C264(G3)	
24	24 Mc/s	NIL		C208(D3)		C263(H3)	
25	25 Mc/s	NIL		C207(A2)		C262(E2)	
26	26 Mc/s	NIL		C206(B2)		C261(F2)	
27	27 Mc/s	NIL		C205(C2)		C260(G2)	
28	28 Mc/s	NIL		C204(D2)		C259(H2)	
29	29 Mc/s	NIL		C203(B1)		C258(F1)	
30	30 Mc/s	NIL		C202(C1)		C257(G1)	

This core is pre-set during initial alignment and will not require adjustment.

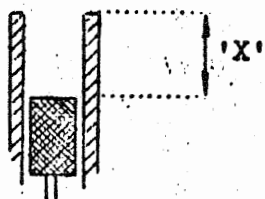
* All cores marked in this way should only be adjusted if it proves

impossible to correctly align (using the appropriate trimmers) all or any of the ranges for which they are used.

If adjustment is required, it will be necessary to set the core(s) by measurement of the depth of penetration into the former (measure from the end remote from the tuning platform) with the tuning control set to centre scale. The Table below gives the correct settings required.

TABLE 9.

Inductance	'X'
L33, 45 and 57	1. 15/16"
L32, 44 and 56	1. 7/8"
L31, 43 and 55	2"
L30, 42 and 54	1. 7/8"



NOTE: The 2nd RF and 1st Mixer trimmers C201 and C256 (marked 'X' in Fig. 5.) should not be touched when carrying out re-alignment. These trimmers are in circuit on all ranges and are used to balance circuit capacities during initial alignment of the receiver. The Aerial Trimmer (panel control) should be set at 'half capacity' on Ranges 1-8, but on the other ranges its ability to resonate the input circuit indicates correct alignment of L30-33.

APPENDIX 'A'

VALVE BASE CONNECTIONS

B7G Types.

Type	Pin Connections						
	1	2	3	4	5	6	7
OB2	A	K	IC	K	A	IC	K
6AK5	G1	K, G3, S	H	H	A	G2	K, G3, S
6AL5	K'	A''	H	H	K''	S	A'
6AM5	G1	K, G3	H	H	A	NC	G2
6BA6	G1	G3, S	H	H	A	G2	K
6BE6	G1	K, G5	H	H	A	G2 & G4	G3
6C4	A	NC	H	H	A	G	K

B9A Types.

Type	Pin Connections								
	1	2	3	4	5	6	7	8	9
6U8	A _t	G1 _p	G2 _p	H	H	A _p	K _p , S G3 _p	K _t	G1 _t
12AT7/12AU7	A''	G''	K''	H	H	A'	G'	K'	H _{tap}

Flying Lead Types. (B8D/F Base)

Type	Pin Connections							
	1	2	3	4	5	6	7	8
EF732	G1	K, G3	H	K, G3	A	H	G2	K, G3

B5B/F Base

6489 (CV469) Anode 2 & 5, Cathode 3, Heater 1 & 4

APPENDIX 'B'

COMPONENT VALUES, TOLERANCES AND RATINGS

Capacitors.

C1	30 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C2	140 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C3	30 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C4	100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
C5	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C6	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C7	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C8	100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
C9	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C10	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C11	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C12	100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
C13	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C14	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C15	400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C16	40 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C17	100 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C18	130 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C19	40 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C20	100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
C21	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C22	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C23	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C24	100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
C25	0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C26	0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
C27	0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
C28	800 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C29	100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
C30	0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
C31	0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.

C32 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C33 6 pF Silvered Ceramic $\pm$ 1 pF 350V DC wkg.
 C34 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C35 1500 pF Silvered Ceramic $\pm$ 20% 350V DC wkg.
 C36 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C37 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C38 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C39 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C40 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C41 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C42 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C43 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C44 1500 pF Silvered Ceramic $\pm$ 20% 350V DC wkg.
 C45 1500 pF Silvered Ceramic $\pm$ 20% 350V DC wkg.
 C46 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C47 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C48 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C49 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
 C50 15 - 150 pF (nominal) Air Spaced Variable.
 C51 2 - 30 pF Air Trimmer.
 C52 Value not yet finalised.
 C53 Value not yet finalised.
 C54 100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
 C55 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C56 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C57 400 pF Silvered Mica $\pm$ 10% 350V DC wkg.
 C58 40 pF Silvered Mica $\pm$ 5% 200V DC wkg.
 C59 100 pF Silvered Mica $\pm$ 5% 200V DC wkg.
 C60 130 pF Silvered Mica $\pm$ 5% 200V DC wkg.
 C61 40 pF Silvered Mica $\pm$ 5% 200V DC wkg.
 C62 1500 pF Silvered Ceramic $\pm$ 20% 350V DC wkg.
 C63 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C64 1500 pF Silvered Ceramic $\pm$ 20% 350V DC wkg.
 C65 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C66 100 pF Silvered Mica $\pm$ 10% 350V DC wkg.

C67 0.01 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C68 300 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C69 770 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C70 970 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C71 300 pF Silvered Mica $\pm$ 5% 200V DC wkg.
C72 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
C73 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
C74 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
C75 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
C76 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C77 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C78 800 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C79 800 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C80 2 - 10 pF Air Trimmer (Differential)
C81 20 pF Silvered Mica $\pm$ 10% 350V DC wkg.
C82 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C83 100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
C84 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C85 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C86 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C87 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C88 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C89 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C90 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C91 100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
C92 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C93 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C94 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C95 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C96 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C97 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C98 400 pF Silvered Mica $\pm$ 2% 350V DC wkg.
C99 100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
C100 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
C101 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.

C102 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
 C103 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
 C104 100 pF Silvered Mica $\pm$ 2% 350V DC wkg.
 C104A 2 pF Ceramic $\pm$ 5% 350V DC wkg.
 C105 40 pF Silvered Ceramic $\pm$ 10% 350V DC wkg.
 C106 100 pF Silvered Mica $\pm$ 2% 350V DC wkg.
 C107 100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
 C108 500 pF Moulded Mica $\pm$ 20% 350V DC wkg.
 C109 0.01 mfd Moulded Mica $\pm$ 20% 350V DC wkg.
 C110 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
 C111 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C112 10 pF Silvered Ceramic $\pm$ 10% 350V DC wkg.
 C113 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C114 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C115 0.5 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
 C116 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
 C117 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C118 0.01 mfd Moulded Mica $\pm$ 20% 350V DC wkg.
 C119 30 mfd Tubular Electrolytic 15V DC wkg.
 C120 0.05 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
 C121 0.5 mfd Tubular Paper $\pm$ 20% 350V DC wkg.
 C122 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C123 500 pF Tubular Paper $\pm$ 20% 350V DC wkg.
~~C124 500 pF Tubular Paper $\pm$ 20% 350V DC wkg.~~
~~C125 5000 pF Tubular Paper $\pm$ 20% 250V DC wkg.~~
 C126 100 pF Silvered Mica $\pm$ 10% 350V DC wkg.
 C127 30 mfd Tubular Electrolytic 15V DC wkg.
 C128 3 - 15 pF Air Spaced Variable.
 C129 100 pF Silvered Mica $\pm$ 2% 350V DC wkg.
 C130 7000 pF Silvered Mica $\pm$ 1% 350V DC wkg.
 C131 7000 pF Silvered Mica $\pm$ 1% 350V DC wkg.
 C132 7000 pF Tubular Paper $\pm$ 20% 350V DC wkg.
 C133 7000 pF Tubular Paper $\pm$ 20% 350V DC wkg.
 C134 7000 pF Tubular Paper $\pm$ 20% 350V DC wkg.
 C135 30 mfd Tubular Electrolytic 15V DC wkg.
 C136 0.01 mfd Moulded Mica $\pm$ 20% 350V DC wkg.
 C124 0.005 Tubular Paper $\pm$ 20% 250V
 C124a 40pF Silvered Mica $\pm$ 10% 350V
 C125 } 500 pF
 C125a }

C137 0.01 mfd Moulded Mica $\pm$ 20% 350V DC wkg.
 C138 30 mfd Tubular Electrolytic 15V DC wkg.
 C139 0.01 mfd Moulded Mica $\pm$ 20% 350V DC wkg.
 C140 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C141 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C142 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C143 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C144 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C145 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C146 0.01 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C147 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C148 1500 pF Silvered Ceramic Feed Thru' $\pm$ 20% 350V DC wkg.
 C149 0.25 mfd Tubular Paper $\pm$ 20% 150V DC wkg.
 C150 50 mfd Tubular Electrolytic 450V DC wkg.
 C151 50 mfd Tubular Electrolytic 450V DC wkg.
 C152 50 mfd Tubular Electrolytic 450V DC wkg.
 C153 0.5 mfd Tubular Paper $\pm$ 20% 150V DC wkg.

C154 - C318 See Detached Circuits 1-5.

Resistors.

R1 0.27 Megohm $\pm$ 10% $\frac{1}{4}$ watt.	R15 270 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R2 12 ohms $\pm$ 20% $\frac{1}{4}$ watt.	R16 2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R3 47,000 ohms $\pm$ 10% 1 watt.	R17 470 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R4 68 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R18 1 Megohm $\pm$ 10% $\frac{1}{4}$ watt.
R5 2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R19 10,000 ohms $\pm$ 10% 1 watt.
R6 0.27 Megohm $\pm$ 10% $\frac{1}{4}$ watt.	R20 47,000 ohms $\pm$ 10% 1 watt.
R7 12 ohms $\pm$ 20% $\frac{1}{4}$ watt.	R21 470 ohms $\pm$ 10% $\frac{1}{4}$ watt.
R8 47,000 ohms $\pm$ 10% 1 watt.	R22 0.27 Megohm $\pm$ 10% $\frac{1}{4}$ watt.
R9 68 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R23 12 ohms $\pm$ 20% $\frac{1}{4}$ watt.
R10 0.1 Megohm $\pm$ 10% $\frac{1}{2}$ watt.	R24 47,000 ohms $\pm$ 10% 1 watt.
R11 47,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R25 68 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R12 2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R26 2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R13 0.27 Megohm $\pm$ 10% $\frac{1}{4}$ watt.	R27 0.27 Megohm $\pm$ 10% $\frac{1}{4}$ watt.
R14 12 ohms $\pm$ 20% $\frac{1}{4}$ watt.	R28 12 ohms $\pm$ 20% $\frac{1}{4}$ watt.

R29	1 Megohm $\pm$ 10% $\frac{1}{4}$ watt.	R64	100 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R30	270 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R65	12 ohms $\pm$ 20% $\frac{1}{4}$ watt.
R31	0.1 Megohm $\pm$ 10% $\frac{1}{4}$ watt.	R66	0.27 Megohm $\pm$ 10% $\frac{1}{4}$ watt.
R32	~~47~~ ⁴⁰ ,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R67	47,000 ohms $\pm$ 10% 1 watt.
R33	2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R68	2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R34	3,300 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R69	0. ~~47~~ Megohm $\pm$ 10% $\frac{1}{4}$ watt.
R35	47,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R70	150 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R36	10,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R71	0.47 Megohm $\pm$ 10% $\frac{1}{2}$ watt.
R37	150 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R72	1 Megohm $\pm$ 10% $\frac{1}{4}$ watt.
R38	68 ohms $\pm$ 10% $\frac{1}{4}$ watt.	R73	1 Megohm $\pm$ 10% $\frac{1}{4}$ watt.
R38 A	~~10 K~~ ^{10 K} $\pm$ 10% $\frac{1}{2}$ W	R74	0.1 Megohm $\pm$ 10% $\frac{1}{2}$ watt.
R39	1000 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R75	2 Megohm $\pm$ 10% $\frac{1}{2}$ watt.
R40	2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R76	0.1 Megohm $\pm$ 10% $\frac{1}{2}$ watt.
R41	0.47 Megohm $\pm$ 10% $\frac{1}{4}$ watt.	R77	0.1 Megohm $\pm$ 10% $\frac{1}{2}$ watt.
R42	150 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R78	10,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R43	2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R79	1 Megohm $\pm$ 10% $\frac{1}{2}$ watt.
R44	47,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R80	1 Megohm $\pm$ 10% $\frac{1}{2}$ watt.
R45	22,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R81	68 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R46	2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R82	2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R47	470 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R83	22,000 ohms $\pm$ 10% 1 watt.
R48	33,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R83 A	~~1 K~~ ^{1 K} $\pm$ 10% $\frac{1}{2}$ W
R49	470 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R84	470 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R50	2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R85	47,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R51	680 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R86	470 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R52	68 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R87	0.47 Megohm $\pm$ 10% $\frac{1}{2}$ watt.
R53	2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R88	0.1 Megohm $\pm$ 10% 1 watt.
R54	10,000 ohms $\pm$ 10% 1 watt.	R89	3,300 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R55	47,000 ohms $\pm$ 10% 1 watt.	R90	0.47 Megohm $\pm$ 10% $\frac{1}{2}$ watt.
R56	0.27 Megohm $\pm$ 10% $\frac{1}{4}$ watt.	R91	47 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R57	47,000 ohms $\pm$ 10% 1 watt.	R92	1000 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R58	2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R93	33,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R59	100 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R94	10,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R60	12 ohms $\pm$ 20% $\frac{1}{4}$ watt.	R95	~~47,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.~~
R61	0.27 Megohm $\pm$ 10% $\frac{1}{4}$ watt.	R96	22,000 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R62	47,000 ohms $\pm$ 10% 1 watt.	R97	220 ohms $\pm$ 10% $\frac{1}{2}$ watt.
R63	2,200 ohms $\pm$ 10% $\frac{1}{2}$ watt.	R98	~~0.47~~ ^{1.0} Megohm $\pm$ 10% $\frac{1}{2}$ watt.

R99	^{1.0} ~~0.18~~ Megohm $\pm 10\%$ $\frac{1}{2}$ watt.	R109	620 ohms $\pm 10\%$ $\frac{1}{2}$ watt.
R100	^{1.8} ~~0.18~~ Megohm $\pm 10\%$ $\frac{1}{2}$ watt.	R110	0.1 Megohm $\pm 10\%$ 1 watt.
R101	0.1 Megohm $\pm 10\%$ $\frac{1}{2}$ watt.	R111	4,700 ohms $\pm 10\%$ $\frac{1}{2}$ watt.
R102	^{3,300} ~~5,600~~ ohms $\pm 10\%$ $\frac{1}{2}$ watt.	R112	10 ohms $\pm 10\%$ 3 watt wirewound.
R102A	^{3.3K} ~~5.6K~~ $\pm 10\%$ $\frac{1}{2}$ watt.	R113	10,000 ohms $\pm 10\%$ 1 watt.
R103	0.1 Megohm $\pm 10\%$ $\frac{1}{2}$ watt.	R114	~~2,200~~ ohms $\pm 10\%$ 6 watt wirewound.
R104	0.47 Megohm $\pm 10\%$ $\frac{1}{2}$ watt.	R115	0.27 Megohm $\pm 10\%$ $\frac{1}{2}$ watt.
R105	2 Megohm $\pm 10\%$ $\frac{1}{2}$ watt.	R116	10,000 ohms $\pm 10\%$ $\frac{1}{2}$ watt.
R106	0.68 Megohm $\pm 5\%$ $\frac{1}{2}$ watt.	R117	140 ohms $\pm 10\%$ 5 watt wirewound.
R107	0.47 Megohm $\pm 5\%$ $\frac{1}{2}$ watt.	R118	140 ohms $\pm 10\%$ 5 watt wirewound.
R108	2 Megohm $\pm 10\%$ $\frac{1}{2}$ watt.		

R118A- R129 See Detached Circuits 1-5.

Potentiometers.

RV1	10,000 ohms wirewound.	RV4	0.5 Megohm carbon.
RV2	10,000 ohms wirewound.	RV5	5 ohms wirewound.
RV3	600 ohms wirewound.		

→ R104 3.3 M $\pm 10\%$ $\frac{1}{2}$ W
 R105 0.47 M " "
 R106 68K $\pm 5\%$ "
 R107 0.47M $\pm 10\%$ "
 R108 3.3 M $\pm 10\%$ "

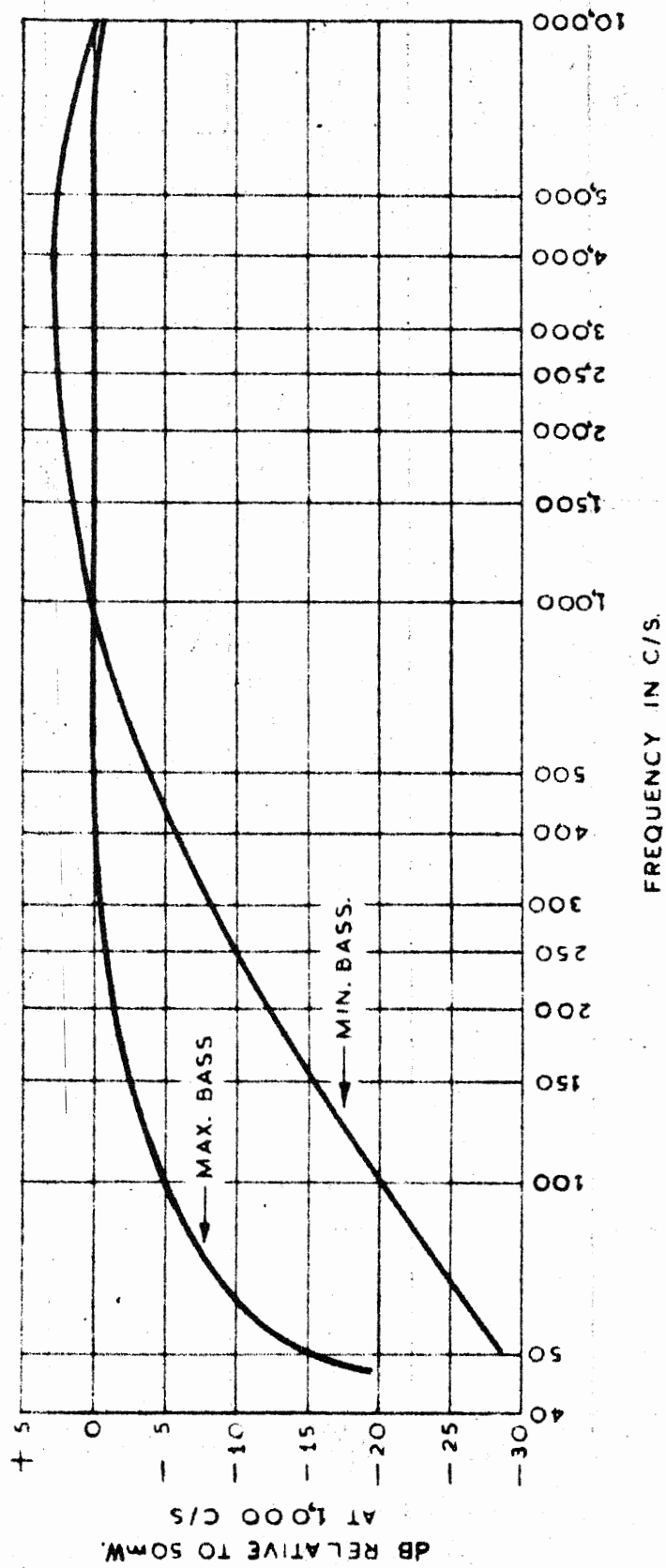


FIG.1. AUDIO RESPONSE IN MAXIMUM AND MINIMUM POSITIONS OF BASS SWITCH.
(AUDIO FILTER OUT OF CIRCUIT AND VOLUME CONTROL AT MAX.)

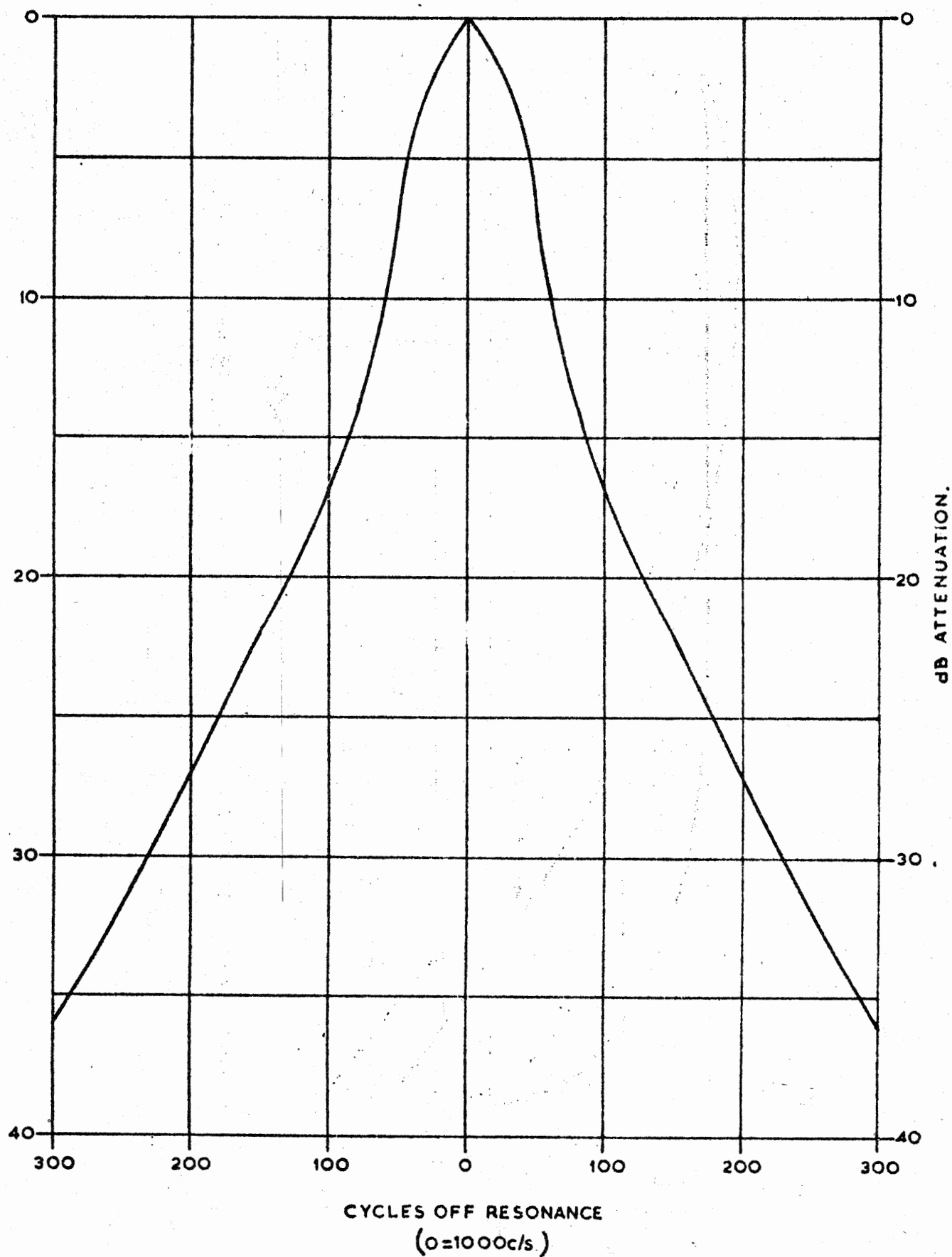
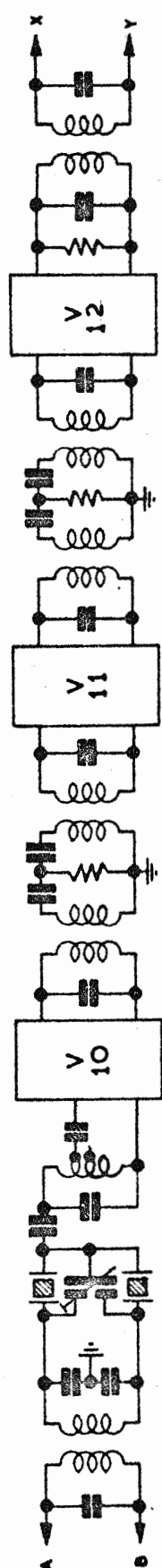
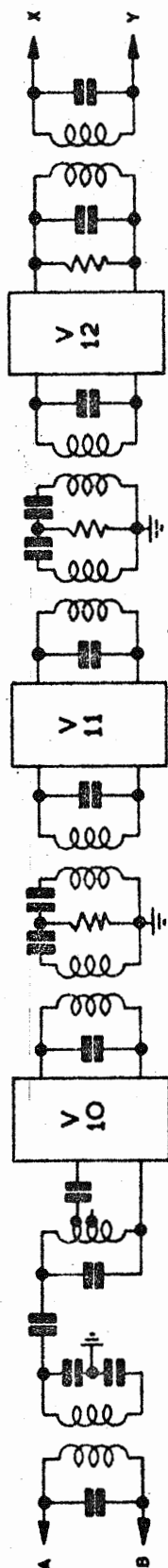


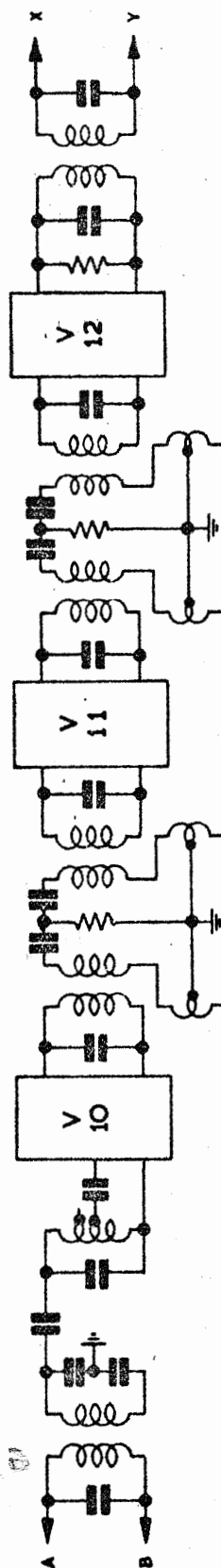
FIG 2 OVERALL SELECTIVITY AUDIO FILTER IN CIRCUIT.



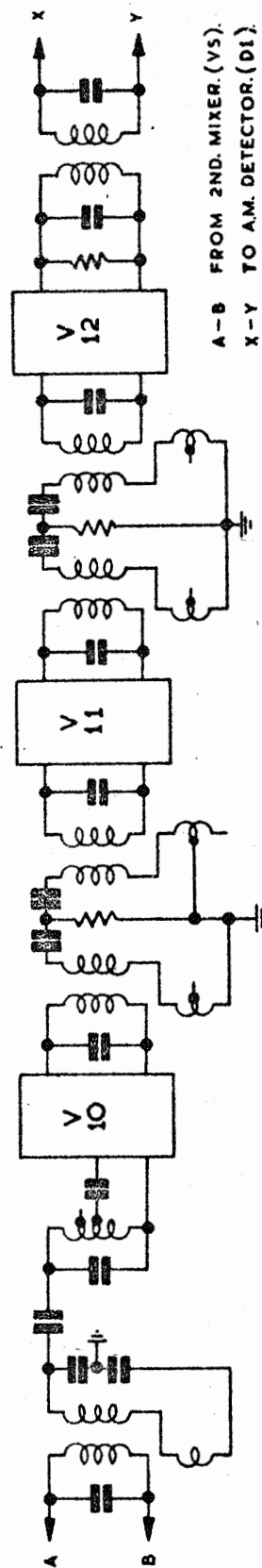
S2 AT POSITION 1 "CRYSTAL WITH AUDIO FILTER" AND POSITION 2 "CRYSTAL".



S2 AT POSITION 3 "NARROW".



S2 AT POSITION 4 "INTERMEDIATE".



S2 AT POSITION 5 "BROAD".

A-B FROM 2ND. MIXER. (VS).
X-Y TO AM. DETECTOR. (DI).

FIG. 4. COUPLING ARRANGEMENTS AT EACH POSITION OF SELECTIVITY SWITCH (S2)

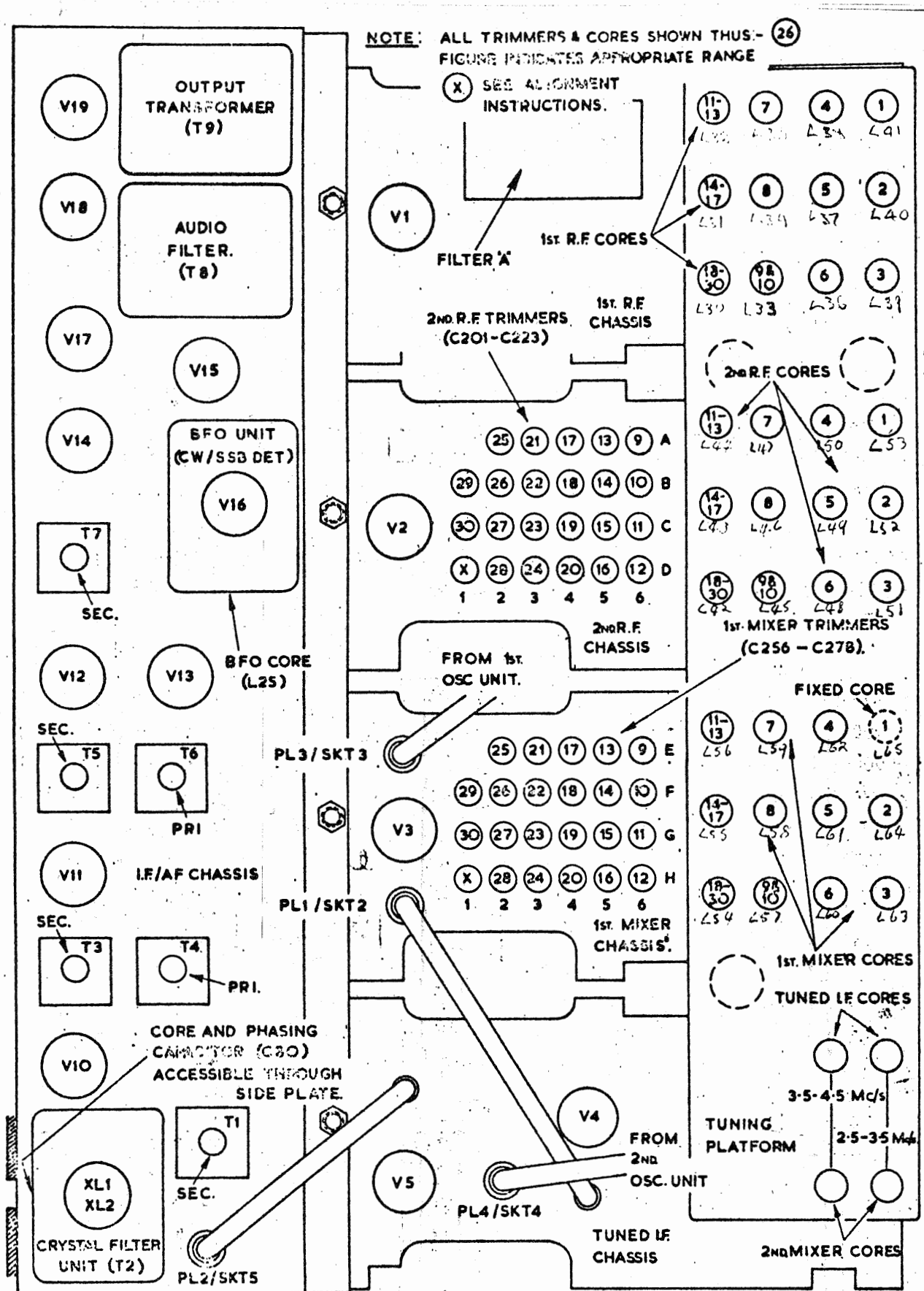
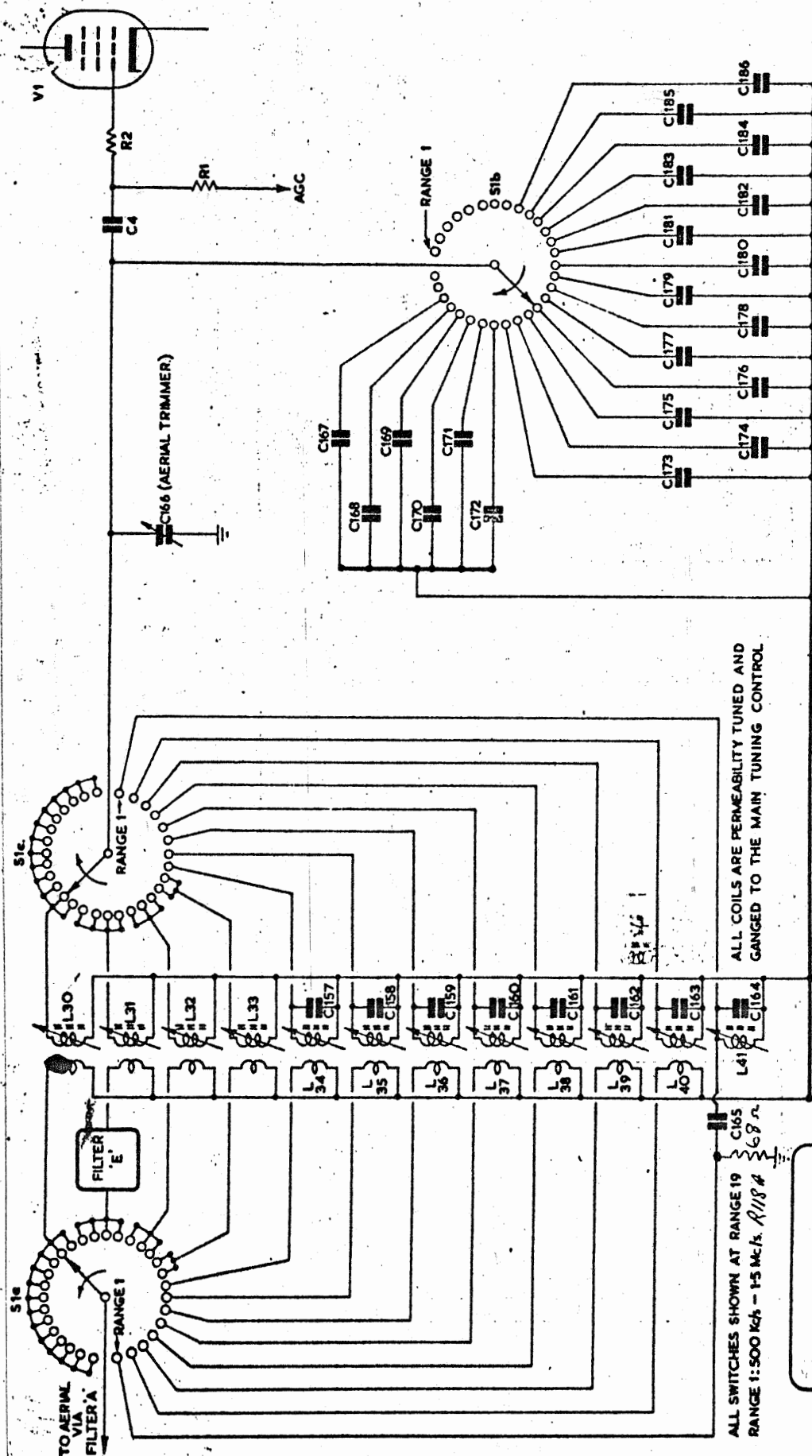
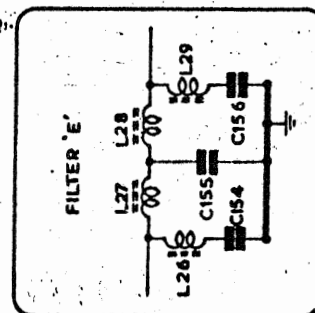


FIG 5 LOCATION OF R.F. AND I.F. TRIMMING ADJUSTMENTS.



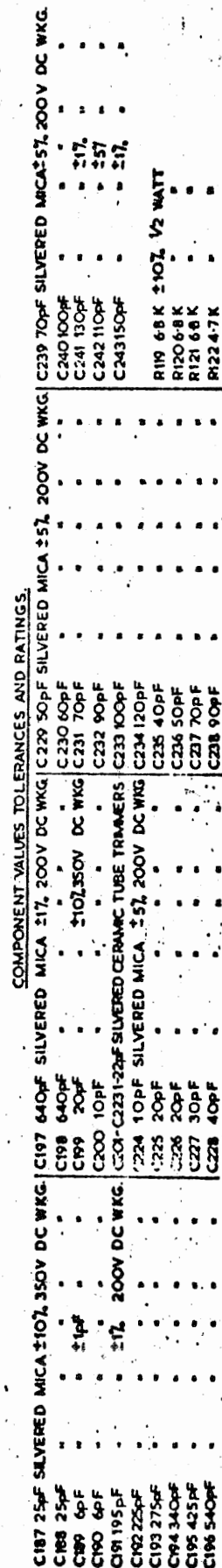
COMPONENT VALUES TOLERANCES AND RATINGS.

C154	60pF SILVERED MICA $\pm 5\%$	200V DC WKG	C165	20pF SILVERED MICA $\pm 10\%$	350V DC WKG	C176	100pF SILVERED MICA $\pm 5\%$	200V DC WKG.
C155	250pF		C166	50pF AIR SPACED VARIABLE		C177	120pF	
C156	60pF		C167	10pF SILVERED MICA $\pm 5\%$	200V DC WKG	C178	40pF	
C157	195pF	$\pm 1\%$	C168	20pF		C179	50pF	
C158	225pF		C169	20pF		C180	70pF	
C159	275pF		C170	30pF		C181	90pF	
C160	340pF		C171	40pF		C182	70pF	
C161	425pF		C172	50pF		C183	100pF	
C162	540pF		C173	60pF		C184	130pF	$\pm 1\%$
C163	640pF		C174	70pF		C185	110pF	$\pm 5\%$
C164	640pF		C175	90pF		C186	150pF	$\pm 1\%$

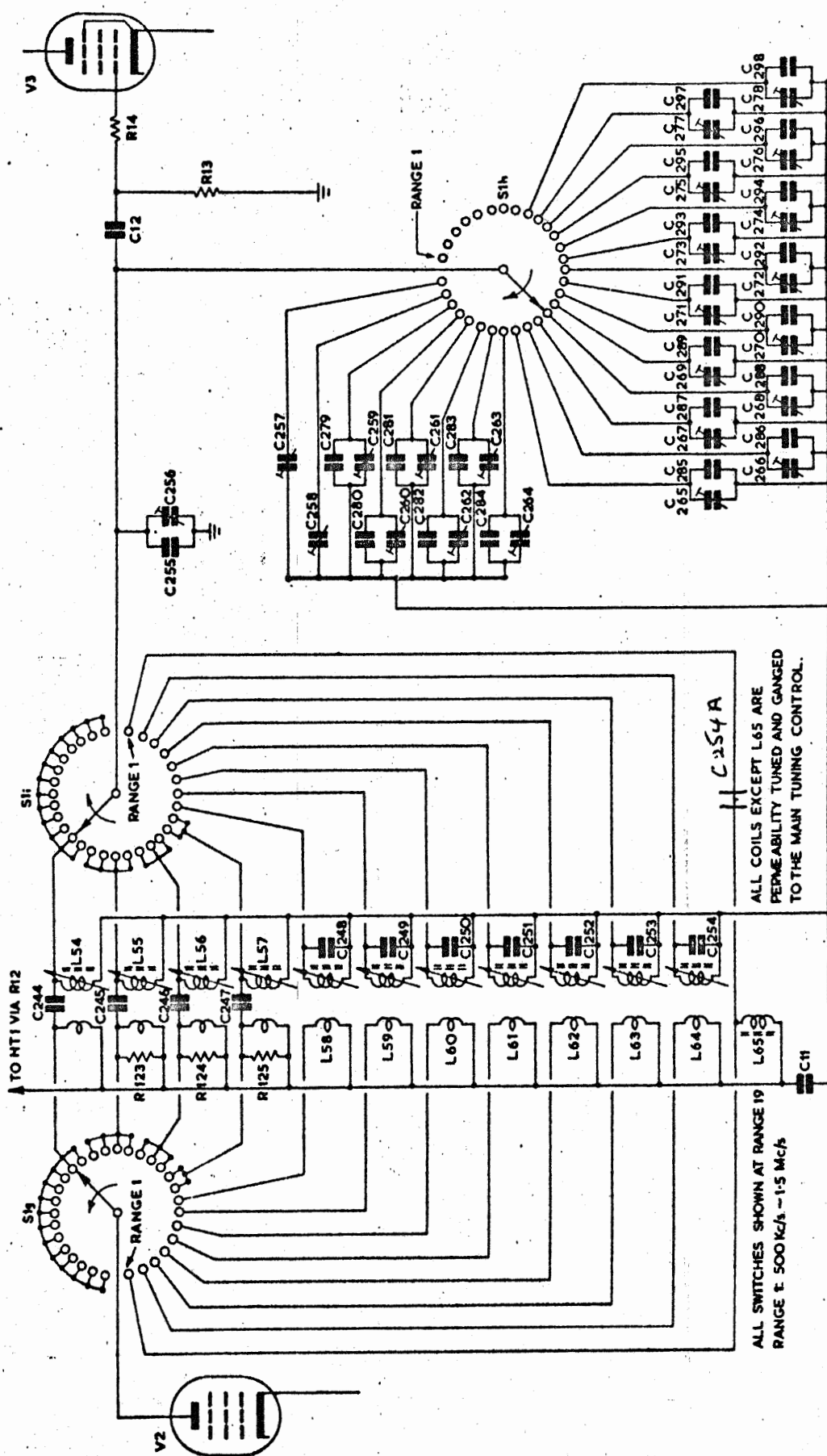


ALL SWITCHES SHOWN AT RANGE 19
RANGE 1: 500 KHz - 1.5 Mc/sec. R118 #

ALL COILS ARE PERMEABILITY TUNED AND
GANGED TO THE MAIN TUNING CONTROL



-50-

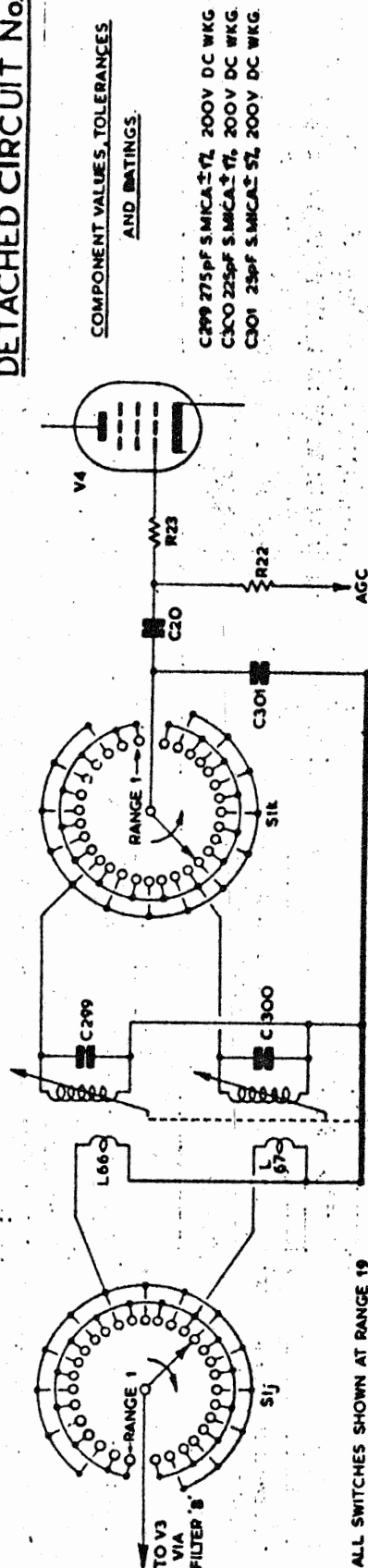


COMPONENT VALUES, TOLERANCES AND RATINGS:

C244 25pF SILVERED MICA $\pm 10\%$, 350V DC WKG	C253 540pF SILVERED MICA $\pm 1\%$, 200V DC WKG	C284 50pF SILVERED MICA $\pm 5\%$, 200V DC WKG	C293 90pF SILVERED MICA $\pm 5\%$, 200V DC WKG
C245 25pF	C254 640pF	C285 60pF	C294 70pF
C246 6pF	C255 10pF	C286 70pF	C295 100pF
C247 6pF	C256-C278 1-22pF SILVERED CERAMIC TUBE TRIMMERS	C287 90pF	C296 130pF
C248 195pF	C279 10pF SILVERED MICA $\pm 5\%$, 200V DC WKG	C288 100pF	C297 110pF
C249 225pF	C280 20pF	C289 120pF	C298 150pF
C250 275pF	C281 20pF	C290 40pF	R123 6-8K
C251 340pF	C282 30pF	C291 50pF	R124 6-8K
C252 425pF	C283 40pF	C292 70pF	R125 6-8K
			10 Ω , V_2 WATT.

DETACHED CIRCUIT No. 3.

DETACHED CIRCUIT No.4.

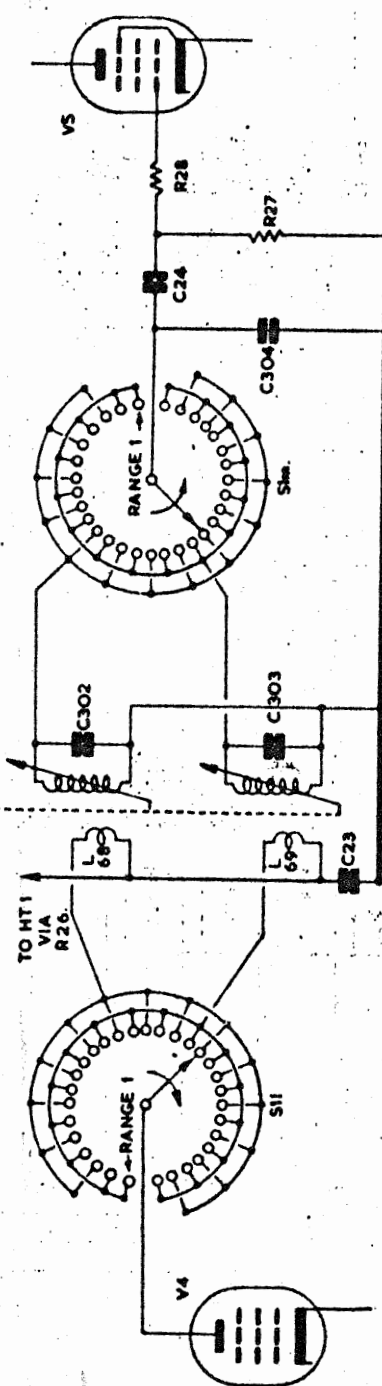


COMPONENT VALUES, TOLERANCES
AND RATINGS

C299 275pF 5MICA±1% 200V DC WKG.
C300 225pF 5MICA±1% 200V DC WKG.
C301 250pF 5MICA±5% 200V DC WKG.

ALL COILS ARE PERMEABILITY TUNED AND
GANGED TO THE MAIN TUNING CONTROL.

ALL SWITCHES SHOWN AT RANGE 19
RANGE 1: 500KC/15 Mc/1.



C302 275pF 5MICA±1% 200V DC WKG.
C303 225pF 5MICA±1% 200V DC WKG.
C304 250pF 5MICA±5% 200V DC WKG.

DETACHED CIRCUIT No.5 (SEE OPPOSITE)

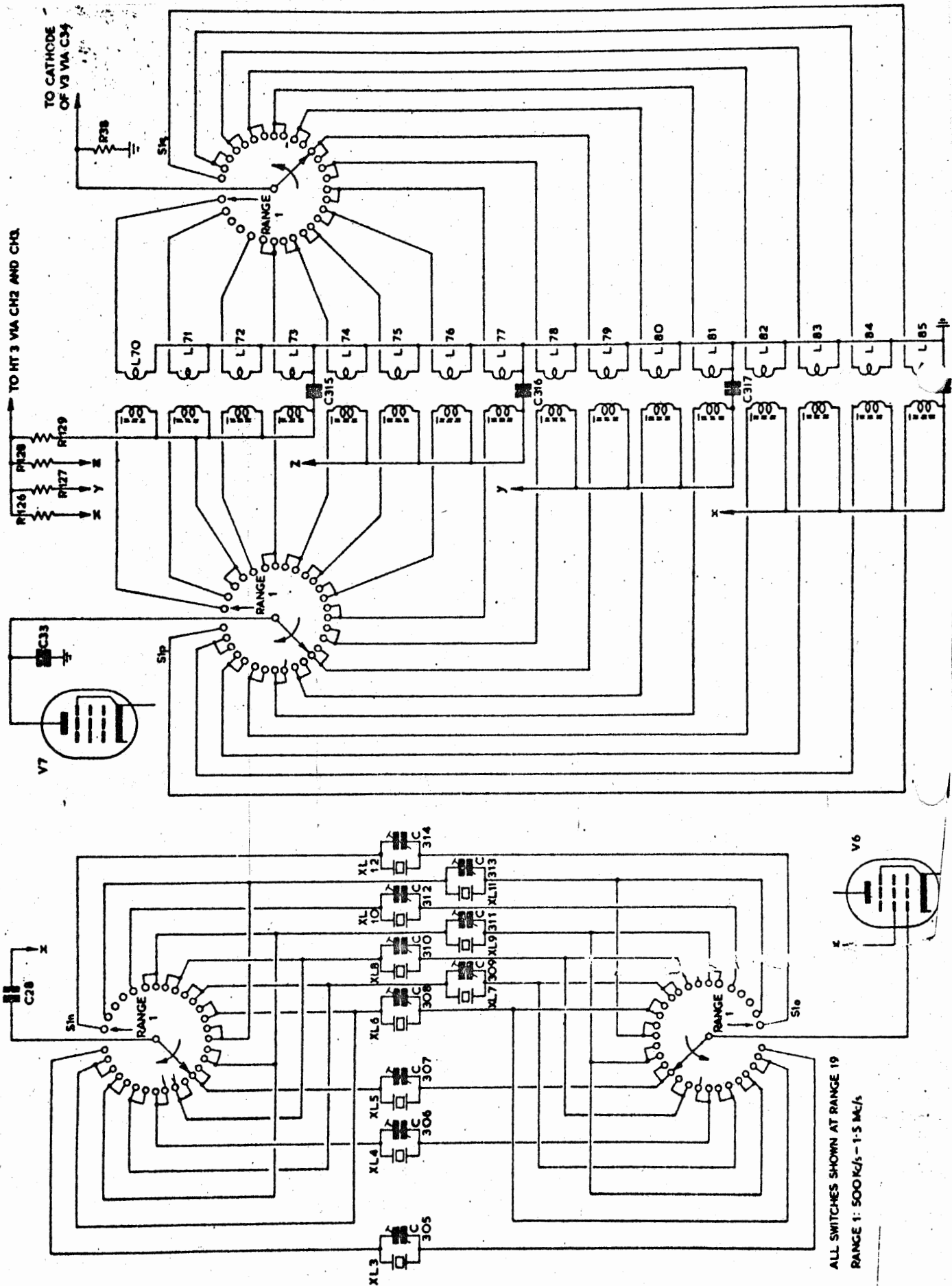
COMPONENT VALUES, TOLERANCES AND RATINGS

C305	1-22pF SILVERED CERAMIC TUBE TRIMMER.
C306	
C307	
C308	
C309	
C310	
C311	
C312	
C313	
C314	

C315	0-01 MFD TUBULAR PAPER 250V 150V DC WKG.
C316	
C317	
C318	

R126	2.2K±10% 1/2 WATT.
R127	
R128	
R129	

XL3	17 Mc/1 INTER-SERVICES STYLE 'D' CRYSTAL UNIT.
XL4	13 Mc/1
XL5	11 Mc/1
XL6	16 Mc/1
XL7	14 Mc/1
XL8	12 Mc/1
XL9	10 Mc/1
XL10	8 Mc/1
XL11	6 Mc/1
XL12	5 Mc/1

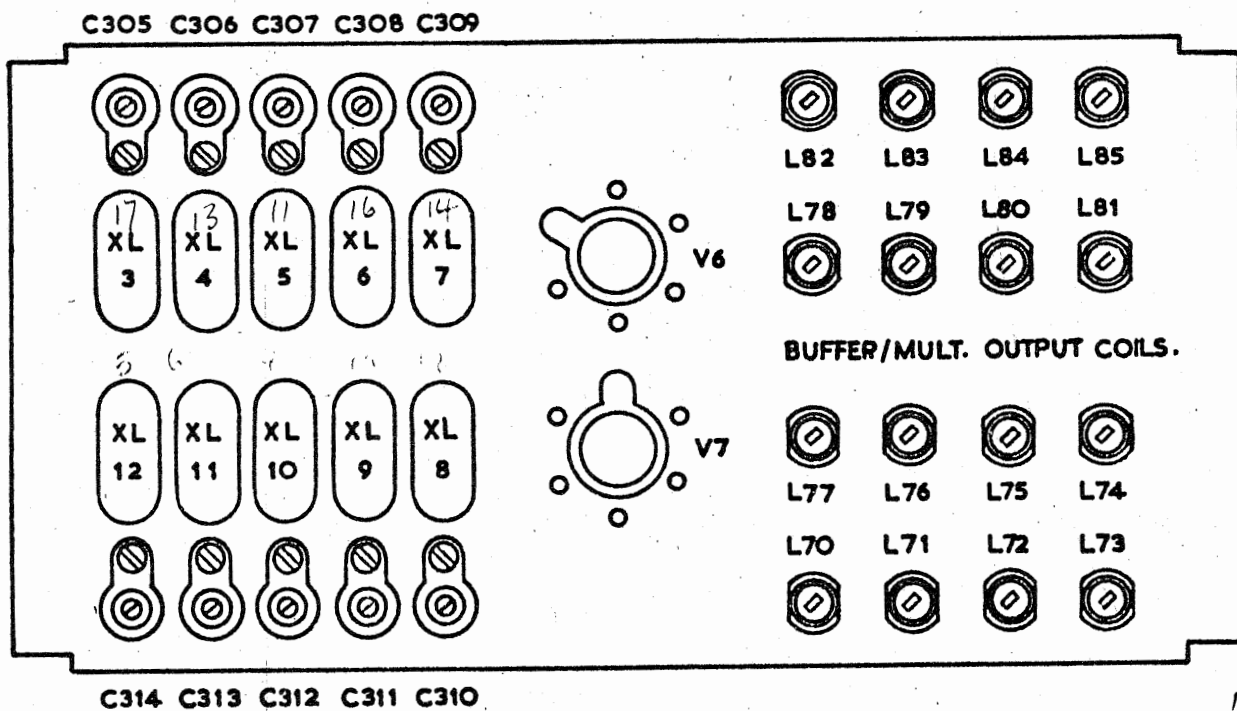


CORRIGENDUM

REVISION OF CRYSTAL POSITIONS (XL3-XL12)

The location of XL3-XL12 given on page 28 is incorrect owing to a modification carried out after the production of this manual.

The revised positioning is given in the diagram below which also shows the location of C305-C314, V6 and V7 and the Buffer/Multiplier output inductances L70-L85



Crystal frequencies are as follows:-

XL3	..	17	Mc/s	XL8	..	12	Mc/s
XL4	..	13	Mc/s	XL9	..	10	Mc/s
XL5	..	11	Mc/s	XL10	..	8	Mc/s
XL6	..	16	Mc/s	XL11	..	6	Mc/s
XL7	..	14	Mc/s	XL12	..	5	Mc/s

