## HANDBOOK FOR <br> REDIFON TYPE R 50 M <br> COMMUNICATIONS RECEIVER

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## CONTENTS

1.0 INTRODUCTION
2.0 DESIGN FEATURES
2.1 Controls and Facilities
2.2 Dimensions and Weights
2.3 Valves
3.0 TYPICAL PERFORMANCE FIGURES
3.1 Sensitivity, Image Discrimination and I.F. Response Ratios
3.2 Selectivity
3.3 Automatic Gain Control
3.4 Stability
3.5 Audio Quality
3.6 Power Consumption
4.0 TECHNICAL DESCRIPTION
4.1 Mechanical Details
4.2 Electrical Details
4.3 Circuit Details
4.3.1 Signal Frequency Amplifier
4.3.2 Oscillator
4.3.3 Mixer
4.3.4 Intermediate Frequency Amplifier
4.3.5 Signal Detector and A.G.C. Rectifier
4.3.6 Beat Frequency Oscillator
4.3.7 Noise Suppressor
4.3.8 Audio Frequency Amplifiex
4.3.9 Manual Gain Controls
5.0 INSTALLATION
5.1 Initial Adjustments
5.2 Fixing the Equipment
5.3 A.C. Mains Supply
5.4 D.C. Mains Supply
5.5 Aerial
5.6 Loudspeaker and Headphones
5.7 Muting
6.0 OPERATION
6.1 General
6.2 Automatic Gain Control
6.3 I.F. Bandwidth
6.4 Logging Scale
6. 5 Standby
6.6 Gain Controls
6.7 Tuning Meter
6. 8 Muting
7.0 MAINTENANCH
7.1 Routine Servicing
7.2 Fault Finding
7.2.1 Power Unit
7.2.2 Audio Frequency Amplifier
7.2.3 Intermediate Frequency Amplifier
7.2.4 Oscillator
7.2.5 Signal Frequency Amplifier and Mixer
7.2.6 A.G.C. and Noise Suppressor
7.2.7 Beat Frequency Oscillator
7.3 Mechanical Adjustments
7.4 Circuit Alignment

## FIGURES

1. A.G.C. Curve
2. $110 \mathrm{kc} / \mathrm{s}$ Crystal Filter
3. Mains Transformer Tappings
4. Muting Circuit Connections

## TABLES

1. Sensitivity, Image Discrimination and I.F. Response Ratios
2. Mains Transformer Connections
3. Service Meter Readings
4. Test Point Voltages and Resistances
5. Signal Amplifier Gains
APPENDIX
I.F. Response Curves
Receiver DiagramComponents List (Receiver)
Power Unit Diagram
Components List (Power Unit)
Inter-connecting Cable
Components lay-out

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## 1.O INTRODUCTION

The Redifon R 50 M is a superheterodyne communications receiver of the highest grade covering the frequency ranges $13.5 \mathrm{kc} / \mathrm{s}$ to $26 \mathrm{kc} / \mathrm{s}$ and $95 \mathrm{kc} / \mathrm{s}$ to $32 \mathrm{Mc} / \mathrm{s}$ in eight bands. (See para 4.3 .1 ) It meets the requirements of Part Two of Second Schedule of the Ministry of Transport Merchant Shipping (Radio) Rules, 1952, and has received the Type Approval Certificate issued by the Post Master General. Both rack mounting and cabinet versions are available.

The receiver has a high discrimination logging scale and employs two stages of signal frequency amplification and a hexode mixer with separate triode oscillator, followed by three stages of intermediate frequency amplification. Owing to the frequency coverage, two of the bands are operated with a different intermediate frequency from the remainder.

Five band widths are available on each of the I.F. channels, crystals being used for the two narrowest. A double diode is employed as an A.G.C. rectifier and signal detector, the latter feeding a pentode amplifier, resistance capacity coupled to the beam tetrode output valve, and a second double diode acts as a noise limiter. The A.G.C. voltage controls the gain of the two R.F. and the first two I.F. amplifiers and a high stability beat frequency oscillator is included for C.W. reception. Muting facilities are available should the receiver be used in conjunction with a nearby transmitter.

The A.C. power unit has the normal full wave rectifier with choke capacity smoothing and features a neon stabilised supply to the oscillator valves and the screen of the frequency changer. For D.C. mains operation, a DC/AC rotary converter is available for use with the A.C. power unit.
2.1 Controls and Facilities

Slow motion and direct tuning controls
Full vision scale and high discrimination logging scale
B.F.C. - Standby - Muting switch

Service meter and switch
A.G.C. - Noise Suppressor switch

Noise Suppressor control
A.F. gain control
R.F. - I.F. gain control

Frequency range switch
Aerial trimmer
B.F.O. control
I.F. bandwidth switch

Full muting facilities available
A.G.C. line taken to output socket so that receiver may be used in diversity
2.2 Dimensions and Weights

Height Width Depth Weight
Chassis only
$12 \frac{1}{2}$ in. 19 in. $21 \frac{1}{2}$ in. $\quad 52 \mathrm{lb}$. $31.8 \mathrm{~cm} .48 .3 \mathrm{~cm} .54 .6 \mathrm{~cm} . \quad 23.6 \mathrm{~kg}$. Cabinet Model

143/4 in. 21 in. $21 \frac{1}{2}$ in. $\quad 89 \mathrm{lb}$. $37.6 \mathrm{~cm} .53 .5 \mathrm{~cm} . \quad 54.6 \mathrm{~cm} . \quad 40.5 \mathrm{~kg}$. A.C. Power Unit

| $6 / 4 \mathrm{in}$. | 17 in. | 7 in. | 25 lb. |
| :--- | :--- | :--- | :--- |
| 15.8 cm. | 43.2 cm. | 17.8 cm. | 11.4 kg. |

2. 3 Valves

V1 and V2, signal frequency amplifiers EF39
V3, frequency changer, ECH35
V4, oscillator, L63
V5, V6 and V7, I.F. amplifiers, EF39
V9, detector and A.G.C. rectifier, EB34 or 6H6
VIO, noise limiter,
V8, B.F.O.,
V1l, A. F. amplifier,
V12, output amplifier,
EB34 or 6H6
EF37A or EF36
EF37A or EF36
6V6G

## Power Unit Valves

V1, Neon stabiliser, S. 130
V2, Rectifier, 5Z4G

Substitution of equivalent types of valves will not cause any marked reduction in performance but where the receiver is installed in a ship subject to the M.O.T. Merchant Shipping (Radio) Rules, 1952, it should be noted that the Type Approval Certificate is granted for the equipment using the types shown above and that the use of others may give rise to difficulties at the Marine Inspector's Survey in U.K. ports.

### 3.0 TYPICAL PERFORMANCE FIGURES

3.1 Sensitivity, Image Discrimination and I.F. Response Ratios
Details of sensitivity, image discrimination and I.F. response ratios are given in the table below. Sensitivity is measured as the input required to give an output of 50 mW with a signal/noise ratio of 10 db on Bandwidth 3. At $22 \mathrm{kc} / \mathrm{s}$ the figures are given for Bandwidth 2. The dummy aerial was 300 pF above $4 \mathrm{Mc} / \mathrm{s}$ and 80 ohms below this frequency. The MCW signal was $30 \%$ modulated at $400 \mathrm{c} / \mathrm{s}$.

| Frequency | CW Sens- <br> itivity | MCW Sens <br> itivity | Image Discrim- <br> ination | I.F. Response <br> Ratios |
| :--- | :--- | :--- | :---: | :---: |
| $25 \mathrm{Mc} / \mathrm{s}$ | $<1.0 \mu V$ | $<1.0 \mu V$ | 40 db | $>100 \mathrm{db}$ |
| $15 \mathrm{Mc} / \mathrm{s}$ | $<1.0 \mu V$ | $1.5 \mu V$ | 51 db | $>100 \mathrm{db}$ |
| $8 \mathrm{Mc} / \mathrm{s}$ | $<1.0 \mu V$ | $2.0 \mu V$ | 71 db | $>100 \mathrm{db}$ |
| $4 \mathrm{Mc} / \mathrm{s}$ | $<1.0 \mu V$ | $2.5 \mu V$ | 92 db | $>100 \mathrm{db}$ |
| $2 \mathrm{Mc} / \mathrm{s}$ | $<1.0 \mu V$ | $2.5 \mu V$ | $>100 \mathrm{db}$ | $>100 \mathrm{db}$ |
| $1500 \mathrm{kc} / \mathrm{s}$ | $1.5 \mu V$ | $5.0 \mu V$ | $>100 \mathrm{db}$ | $>100 \mathrm{db}$ |
| $600 \mathrm{kc} / \mathrm{s}$ | $1.5 \mu V$ | $4.0 \mu V$ | 94 db | 85 db |
| $250 \mathrm{kc} / \mathrm{s}$ | $5.0 \mu V$ | $18.0 \mu V$ | $>100 \mathrm{db}$ | $>100 \mathrm{db}$ |
| $100 \mathrm{kc} / \mathrm{s}$ | $4.0 \mu V$ | $15.0 \mu V$ | $>100 \mathrm{db}$ | $>100 \mathrm{db}$ |
| $22 \mathrm{kc} / \mathrm{s}$ | $3.0 \mu V$ | - | $>100 \mathrm{db}$ | 75 db |

Sensitivity, Image Discrimination and I.F. Response Ratios

## Table 1

### 3.2 Selectivity

$110 \mathrm{kc} / \mathrm{s}$ I. F .
Attenuation. Typical overall Bandwidths in kc/s. Switch position

|  |  |  | 1 | 2 | 3 | 4 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 6 db | $\ldots$ | - | 1.2 | 4 | 10 | 12 |
| 30 db | $\ldots$ | 1 | 4.5 | 8 | 13 | 16 |
| 60 db | $\ldots$ | 6 | 8 | 12 | 18 | 21 |

$465 \mathrm{kc} / \mathrm{s}$ I. F .
Attenuation. Typical overall Bandwidths in kc/s. Switch position

|  |  | 1 | 2 | 3 | 4 | 5 |
| :---: | :---: | :---: | :---: | :---: | :---: | ---: |
| 6 db | $\ldots$ | - | 1.2 | 4.5 | 12 | 17 |
| 30 db | $\ldots$ | 0.8 | 4 | 11 | 20 | 25 |
| 60 db | $\ldots$ | 6 | 8 | 18 | 27 | 32 |

I. F. response curves will be found in the appendix to this handbook.

### 3.3 Automatic Gain Control

The shape of the A.G.C. characteristic is shewn in Figure 1 , and was measured at $2 \mathrm{Mc} / \mathrm{s}$ on Bandwidth 3.

An increase in the input of 2 db results in an improvement in the Signal/Noise Ratio of approximately 19 db .

A. G. C. Curve

Figure 1

The time constants on "A.G.C." are approximately O. 1 seconds charge and discharge. On "N.S.-A.G.C." they are 0.1 and 1.0 seconds respectively.

### 3.4 Stability

Between five and ten minutes after switching on, the oscillator frequency does not change by more than
one part in $10^{4}$ over the range 1.5 to $25 \mathrm{Mc} / \mathrm{s}$. Below $1.5 \mathrm{Mc} / \mathrm{s}$, stability is of the order of 3 parts in $10^{4}$ and the drift is negligible after this time. Supply fluctuations of up to $5 \%$ do not affect these figures.
3.5 Audio Quality

The total harmonic distortion is less than $5 \%$ at 2 watts output and the hum level is at least 55 db below this figure.

The response is within 3 db from $250 \mathrm{c} / \mathrm{s}$ to $4000 \mathrm{c} / \mathrm{s}$.
3.6 Power Consumption

The A.C. Power Unit consumes approximately 80 watts.
4.0 TECHNICAL DESCRIPTION
4.1 Mechanical Details

The basic chassis is designed to provide a strong light framework supporting the various units into which the receiver is divided, but which need not be disturbed for normal maintenance or servicing. The front panel is of $1 / 4$ inch aluminium plate and assists in producing a rigid structure.

The sub-assemblies are as follows:-
(a) The I.F. unit, comprising the components for both the I. F. channels and their associated switches mounted in the main chassis on the right hand side.
(b) The output stage, which is mounted in the main chassis, immediately behind the front panel.
(c) The aerial stage, R.F. amplifiers, oscillator and mixer units are mounted side by side and a light alloy casting of generous dimensions, on which the tuning condenser is mounted, is bolted across them. The whole is flexibly mounted to prevent the transference of any shocks or vibrations.

The complete chassis is housed in a sheet metal cabinet finished in grey crackle enamel. It has a flush hinged lid with quick release catch and openings at the rear for access to the input and output sockets.

The power unit is simple and robust, all the components being mounted on one chassis with an aluminium cover.

### 4.2 Electrical Details

All the components and wiring in the receiver and power unit comply with the normal Colonial and Service tropical requirements. No electrolytic condensers are used at high voltages, ceramic switch wafers and insulators are employed in critical circuits, and wiring is either bare tinned copper or insulated with P.V.C. or Polythene. The materials used in the framework and chassis are chosen and finished to produce the minimum contact potentials (not greater than 0.3 volts between adjacent metals).

### 4.3 Circuit Details

### 4.3.1 Signal Frequency Amplifier

Two stages of signal frequency amplification provide a degree of selectivity prior to the mixer stage, reducing cross modulation and blocking by strong interfering signals. At the same time, the higher signal level at the grid of the mixer valve, at which point circuit noise is chiefly introduced in a superheterodyne receiver, results in a considerable improvement in the overall'signal/noise ratio.

The grid circuit of valve Vl and the grid/anode circuits of valves V1, V2 and V2, V3 each employ eight transformer couplings to cover the frequency range of the receiver and all coils not in use are short circuited by the range switch. The secondaries of the transformers are tuned by sections of the double four gang variable condenser, two sections in parallel being used on the long and medium wave bands $D$ to $H$ and one section only on the short wave bands $A$ to $C$. Two series tuned I.F. circuits are provided, when the receiver is on bands $E$ and $G$, to improve I.F. rejection.

The frequency bands are:-

| Band A | $15.5-32 \mathrm{Mc} / \mathrm{s}$ |  |
| :---: | :---: | :---: |
| " | B | $7.7-16 \mathrm{Mc} / \mathrm{s}$ |
| " | C | $3.8-8 \mathrm{Mc} / \mathrm{s}$ |
| " | D | $1.5-4 \mathrm{Mc} / \mathrm{s}$ |
| " | F | $585-1550 \mathrm{Kc} / \mathrm{s}$ |
| " | F | $240-600 \mathrm{Kc} / \mathrm{s}$ |
| " | G | $95-250 \mathrm{Kc} / \mathrm{s}$ |
| " | H | $13.5-26 \mathrm{Kc} / \mathrm{s}$ |

Inductance and capacity trimming is provided in each tuned circuit, with the exception of the aerial coils, which have no capacity trimmers apart from the common aerial trimming condenser. The latter has a control on the front panel of the receiver and tunes the aerial coupling circuit which is designed for use with an 80 ohm unbalanced input on bands $A B$ and $C$ and an aerial of between 200 and 600 pF on the other. bands. It is thus suitable for use with a ships open wire aerial.

### 4.3.2 Oscillator

The first heterodyne oscillator valve V4, is aligned to track with the signal frequency amplifier at a frequency $110 \mathrm{kc} / \mathrm{s}$ higher on bands $H$ and $F$ and $465 \mathrm{kc} / \mathrm{s}$ higher on bands $G, E, D, C, B$ and $A$.

A separate oscillator valve is emplozed with a tuned grid circuit controlled by one or two sections of the rear unit of the ganged variable condenser. One section is employed on range $A$, two sections on ranges B to H .

Radiation from the oscillator is reduced to a very low level by isolating the signal frequency and oscillator circuits.

Inductance as well as capacity trimming is provided in all tuned circuits and on ranges $D$ to $H$ the padder condensers have trimmers.

In order to compensate for changes of temperature and improve frequency stability, condensers with a negative temperature co-efficient are connected in parallel with the grid coils and padding condensers, and in addition a temperature compensated stage is included between oscillator and mixer.

Frequency variations due to mains supply fluctuations are minimised by the stabilised H.T. supply.

### 4.3.3 Mixer

The mixer valve $V 3$ is a triode hexode with a stabilised supply to the screen, the output of the oscillator being fed to the appropriate electrode via the grid of the triode section. The latter is used to reduce warm-up drift in conjunction with the thermistor between grid and cathode.

> 4.3.4 Interme diate Freguency Amplifier

Three stages of I.F. amplification are provided by the variable mu R. F. pentodes $V 5$, $V 6$ and $V 7$. Due to the coverage, it has been necessary to provide two channels at different irequencies and the appropriate one is automatically selected by the range switch.

Selectivity may be varied by means of the switch S. 5 Five bandwidths are available ranging from "Xtal" to "Broad".
(See Appendix for response curves)

The narrow bands employ high stability vacuum mounted crystals as coupling elements between the first I.F. amplifier and the mixer.

$110 \mathrm{kc} / \mathrm{s}$ Crystal Filter

## Figure 2

Figure 2 shows the $110 \mathrm{kc} / \mathrm{s}$ crystal filter when the selectivity switch is in Posn 1 . The changes when it is moved to Posn. 2 are indicated but for simplicity, the switches themselves are not shown.

The voltages induced in the secondary of the I.F. transformer are 180 degrees out of phase at the points $A$ and $B$ and if the preset phasing condenser is adjusted so that its capacity is equal to the crystal holder capacity, there will be no signal at C. At the resonant frequency, however, the crystal behaves as though it has a low resistance in parallel with it (say $5 \mathrm{~K} \Omega$ ) and in this case there will be a resultant output which is fed to the lst I.F. valve via the 150 pF condenser.

In Posn. 2, the crystal damping coil in parallel with the two condensers is introduced between the point $C$ and earth and this has the effect of widening the response.

In Posn. 3, the crystal filter is removed completely, and in Posns, 4 and 5 the response is still further widened by increasing the coupling of the I.F. transformers, of the second and third stages. The 465 $\mathrm{kc} / \mathrm{s}$ channel is similar, but the filter employs two crystals.

### 4.3.5 Signal Detector and A. G. C. Rectifier

One side of the double diode $V 9$ is connected to the secondary of the final I.F. transformer and acts as the signal detector while the other side is connected to the anode of the final I.F. valve and produces delayed A.G.C. voltage controlling the R.F. valves and the first two I.F. valves.

### 4.3.6 Beat Frequency Oscillator

The second heterodyne oscillator V8 is of the electron coupled variety and is coupled to the detector by a 10 pF condenser.

A trimmer condenser with a control on the front panel, trims the beat note to the desired audio frequency and a negative coefficient condenser results in high stability.
4.3.7 Noise Suppressor

Noise suppression may be introduced with or without A.G.C. and is obtained by means of a double diode limiter circuit of the shunt series type. V 10 is the valve used. On CW and when the $465 \mathrm{kc} / \mathrm{s}$ channel is in use a bias is applied to the diode anode which improves the signal/noise ratio.

### 4.3.8 Audio Frequency Amplifier

The voltage amplifier valve V1l. is resistance capacity coupled to the output valve V 12. Negative feedback is introduced to reduce distortion and effective output impedance.

The output valve is of the beam tetrode type and will deliver 2 watts into a 3 or 12 ohm load, the secondary of the output transformer being split into two separate sections of 3 ohms each, for connection in series or parallel. The 12 ohm arrangement constitutes a satisfactory low impedance source for feeding a 600 ohm line. A telephone jack is permanently connected across one winding of the output transformer with a 680 ohm series limiting resistor to give an output suitable for use with headphones of 50 to 120 ohms resistance.

> 4.3.9 Manual Gain Controls

There are two manual controls for adjustment of audio and RF/IF gain.

The audio control, which is used to adjust the output level of the receiver, varies the input to the grid of the first audio amplifier valve vil.

The RF/IF control adjusts the gain of the signal frequency stages and also that of the first two I. F. stages by varying the cathode resistance and hence the bias of these four valves.

### 5.0 INSTALILATION

### 5.1 Initial Adjustments

The receiver and interconnecting cable are packed in a carton; for export packing this is protected by a wooden case, lined with shock absorbing material, also containing the power unit. Having unpacked the equipment proceed as follows:-

If the receiver is supplied in a cabinet
(a) Remove the six front panel retaining screws.
(b) Poll the chassis forward by means of the knobs provided.
(c) Remove the transit brecket, which is temporarily fitted to prevent undue movement of the main sub-assembly during shipment. Four screws hold the bracket to the angle bracket on the front panel and two hold it to the centre screen on the sub-assembly. Replace the latter in the centre screen after removal of the bracket.
(d) Check that all valves are firmly in their sockets.
(e) Remove the power unit cover by withdrawing the four screws at the back and the one on top, adjust the mains voltage tapping (see para 5.3) and replace the cover.

## If the receiver is supplied for 19 inch rack mounting.

(a) Remove the two retaining screws at the back and slide off the top section of the cover.
(b) Remove the transit bracket, temporarily fitted to prevent undue movement of the main sub-assembly during transit. Four screws hold the bracket to the angle bracket on the front panel and two hold it to the centre screen on the sub-assembly. Replace the two in the centre screen.
(c) Check that all valves are firmly in their sockets.
(d) Remove the power unit cover by withdrawing the four screws at the back and the one on top, adjust the mains voltage tapping (see para 5.3 over) and replace the cover.
5.2 Fixing the Equipment.

The R 50 M is mechanically very rigid but it is well to take care that the four rubber feet take the weight evenly when the receiver rests on a bench, to remove the possibility of distortion. It may be held in position by replacing the bolts for the rubber feet by longer bolts or wood screws into the bench.

When mounted in a rack, adequate support must be provided by angle runners or other devices, to take the chassis weight evenly along each side. The six front panel screws are to be used only for holding the receiver to the framework, not for taking its weight.

The power unit may be placed under the bench or in any other convenient position. For rack mounting, it has the standard 19 inch panel and is secured by four screws.
5.3 A.C. Mains Supply

Check that the voltage and frequency of the supply is within the range covered by the power unit and adjust the mains transformer taps as shown in the table below. All power units are adjusted for 240 volts working before leaving the works.

The values of the fuses $F 1$ and $F 2$, to be inserted into the fuse holders, are dependent upon the supply voltage and are 1 amp for 200 to 250 volts and 2 amp for 100 to 125 volts. The H.T. fuse $F 3$ should be 250 mA , in each case.

Connect the receiver to the power unit by means of the interconnecting cable provided. The plug end of the cable is inserted into the socket at the back of the power unit marked P.O. and the socket should be mated with the plug marked R.I. at the back of the receiver.

The mains input plug is on the right hand side of the power unit, viewed from the .rear.


Mains Transformer Tappings
Figure 3

| Mains Volts | Interconnections |  |  |  |  |  | Connect | Mains | Wires | $s$ to |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 0 | to | 0 | and | 100 | to 100 |  | 0 and | 100 |  |
| 105 | 5 | to | 5 | 1 | 100 | " 100 |  | 5 " | 100 |  |
| 110 |  | to | 0 | " | 110 | * 110 |  | 0 " | 110 |  |
| 115 |  | to | 5 | " | 110 | " 110 |  | 5 " | 110 |  |
| 120 | 0 | " | 0 | " | 120 | - 120 |  | 0 " | 120 |  |
| 125 | 5 |  | 5 | " | 120 | . 120 |  | 5 " | 120 |  |
| 200 |  |  | O to | O 10 | 100 bo | ttom |  | bottom | 100 | top |
| 205 | 5 |  | n | 10 | 100 | " | 0 | "1 | 100 | to p |
| 210 |  | " | " |  | 100 | " | 0 | 1 | 110 | top |
| 215 | 5 |  | " | 1 | 100 | 11 | 0 | : | 110 | top |
| 220 | 0 | " |  | 1 | 100 | " | 0 | " | 120 | top |
| 225 | 5 | " | " | 1 | 100 | 1 | 0 | * | 120 | top |
| 230 |  | 1 |  |  | 120 | " | 0 | " | 110 | top |
| 235 | 5 | " | " | 1 | 120 | " | 0 | " | 110 | top |
| 240 |  |  |  |  | 120 | \% | 0 | " | 120 | top |
| 245 | 5 | " | " | 1 | 120 | n | 0 | * | 120 | top |
| 250 | 5 | " | " | 1 | 120 | 1 | 5 | " | 120 | top |

Mains Transformer Connections
Table 2

### 5.4 D.C. Mains Supply

For D.C. mains, the A.C. power unit is used with a D.C. to A.C. rotary converter capable of providing a power of approximately 120 . Watts at 220 volts $50 \mathrm{c} / \mathrm{s}$. D.C. to A.C. converters for 24,110 or 220 volts can be supplied as standard and units for other voltages are available to special order.

When the equipment is to be fitted in British Registered Vessels under the Merchant Shipping Rules 1952, approved type machines must be specified. The following machines, supplied by Redifon, meet the requirements:-

| 24 volts D.C. input | Type No. RED 3 |
| :--- | :--- |
| Il0 volts D.C. input | Type No. RED 4 |
| 220 volts D.C. input | Type No. RED 5 |

It is important to check that the input taps on the mains transformer of the A.C. power unit are adjusted to the voltage output of the converter. This is usually 230 volts. Filters suppressing commutator interference are fitted on the machines.

### 5.5 Aerial

The receiver will function satisfactorily with any normal open wire aerial of between 25 and 250 feet in length and a normal earth connection.

Above $4 \mathrm{Mc} / \mathrm{s}$ it is designed to match an aerial of 80 ohms impedance. (see para 4.3).

The lead in should be passed through the hole in the back of the receiver and connected by means of the co-axial plug and socket mounted at the rear. The earth connection is also made at the rear of the unit.

There is no objection to a co-axial type aerial input being run from a single ended aerial switch, permitting the main transmitting aerial of a ship to be switched to the receiver for long distance working on the very low frequency band.
5.6 Loudspeaker and Headphones.

When a loudspeaker is used with the receiver, connections from the speech coil are taken from Pins 1 and 3 on the 12 way plug at the rear of the set. The loud speaker supplied by Redifon has a 3 ohm resistor which is connected when the speaker is switched off. This is necessary in order to avoid excessive voltages in the output transformer.

For an aidio output of 3 ohms impetance, join terminals $B$ to $D$ and $A$ to $C$ on the output transformer, which is situgted in the power unit.

For 12 ohms impedance join terminals $B$ to $C$ on the output transformer. This may also be used for a 600 ohms line.

A headphone jack socket is provided on the front panel of the recelver for headphones of 120 ohms resistance. It is essential that the reaistance is correct. The use of a high resistance will result in a consilerable reduction in sensitivity.

A 22000 ohms reaistor R2 is connected across the primary winding of the output transformer to minimise the risk of lamage should the receiver be operated under no load conditions. Receivere prior to Serial No. 802 may be without this and it is recommended that such are modified in accordance with the power unit diagram and components list included at the end of this handbook.

### 5.7 Muting

A Redifon Relay Unit is available to provide muting facilities when the receiver forms part of a main installation and is used in conjunction with a transmitter

The circuit diagram of this unit is given overleaf. Muting is accomplished by earthing the screen supply line and receiving aerial during "mark" periods, the change-over being performed by the contacts of relays 1 and 2 respectively, both energised from a D.C. supply when the telegraph key or "press-to-talk" switch is depressed for transmission. The screen supply line is taken to earth via a variable resistor Rl, thus afforing a convenient control of received volume when monitoring out-going transmiseions.

There the recelver is operated from an A.C. mains supply, a D.C. voltage of $12,24,110$ or 220 V must be proviled for energising relays 1 and 2.


## Figure 4 - Muting Circuit Connections

NOTE
For 12 volts D.C. supply - Link A in position.
For 24 volts D.C. supply - Replace Link A with resistor R2.

For 110 volts D.C. supply - Replace Link $A$ with resistor R3.

For 220 volts D.C. oupply - Replace Link $A$ witis resistor R4.

Unless otherwise specified the 24 volts unit is supplied.

Components List.

| Ref: | Value | Description | Remariks |
| :---: | :---: | :---: | :---: |
| C. 1 | 0.001uF | Condenser CM20N $20 \%$ | Ex T.C.C. |
| C. 2 | $0.001 u \mathrm{~F}$ | Condenser CM2ON 20\% | Ex T.C.C. |
| L. 1 |  | Choke H.F.SW 68 | Ex Bulgin |
| R. 1 | 50000hm | Pot. HNAR 50250 | Ex Morganite |
| Rel | 2500hm | High speed relay H88T | Ex Siemens |
| Rel | \% 2500 hm | High speed relay H88T | Ex Siemens |
| R. 2 | 4700 hm | 3/4 watt | Ex Erie |
| R. 3 | 3.9 Kohms | 6 watt Resistor AW3111 | Ex Welwyn |
| R. 4 | 8.2Kohms | 10 watt AW 3112 | Ex Welwyn |

6.0 OPERATION

### 6.1 General

Thurn the switch below the meter to "C.W." for continuous wave working or to "MOD" for telephony and M.C.W. The dial lamps will indicate that the set is switched on and a period of five minutes should be allowed for the valves to warm up and the R.F. circuits to stabilise. If there is a rotary converter, this should be switched on first.

Set the A.G.C. NOISE SUPPRPSSOR Switch to "MAN." i.e. Manual gain control.

Switch the I.F. Bandwidth Control to Posn. 3.
Adjust the RF/IF Gain Control to maximum and the AF gain to give a reasonable noise level.

Turm the range switch to the band required.
Tune in the signal using the large knob for coarse adjustment and the small one for fine. For C.W., rotate the B.F.O. trimmer knob until the pitch of the beat note is satisfactory.

Rotate the Aerial Trimmer for maximum signal.
The I.F. bandwidth switch should now be adjusted to give the required degree of selectivity as detailed in para 6.3.
A.G.C., with or without noise suppression, may now be switched in, using the A.G.C.- N.S. switch and the suppressor control adjusted. Turm the N.S. control fully anti-clockwise and then advance it until the signal to noise ratio is at its optimum, or until distortion begins to appear. The noise suppressor should be used, however, onily if conditions make it necessary.

If muting of the receiver is required, turn the switch under the meter to "Muting C. W." for continuous wave reception, or to "Muting Mod." for telephony.

### 6.2 Automatic Gain Control.

Maximum use should always be made of the A.G.C. since, not only does this circuit ensure that the output remains comparatively unchanged over a: wide range of input levels, but it also improves the signal/noise ratio with any increase in input.

The exception to the use of A.G.C. is when listening to weak or elusive signals accompanied by static or signals of greater field strength, when the interference will operate the A.G.C. and this may reduce the gain sufficiently for the wanted signal to be lost altogether.

## 6. 3 I.F. Bandwidths

Five bandwidths are provided on each of the two I.F. channels, ranging from Posn. 1, Xtal to Posn. 5, Broad, on the bandwidth switch. The latter should be set to Posn. 3, when searching on the lower frequency ranges and to Posn. 4. on the higher ones.

The two narrow bands give a high degree of selectivity for use on C.W. reception or whenever freedom from interfering signals on an adjacent frequency is required. Their use is not recommended for tele phony.

The third position of the switch is suitable for the reception of C.W. under clear conditions and also for telephony subject to strong adjacent channel interference.

Posn. 4 should be used for telephony when some interference is experienced or when the signal is not strong, and Posn. 5 gives the best quality with strong signals.

### 6.4 Logging Scale

A spring loaded gear mechanism is employed and the logging scale is made up of two parts, a fixed coarse scale divided into twenty four parts and traversed by the hair line on the cursor, and a scale of one hundred divisions which rotates once for each division of the coarse scale. There is thus a total of 2400 divisions over each frequency range.

To log a station, the fixed scale should be read first and then the rotating one. The same order of operations should be used when resetting.

### 6.5 Standby

If the receiver is operated for long periods on intermittent duty, it should not be switched off but left on the "Standby" position. This ensures maximum stability and freedom from frequency drift which would arise from the warming up and cooling down of the valves and other components.

### 6.6 Gain Controls

When receiving C.W. or telephony with A.G.C. in use, the RF/IF gain control should be set at maximum for all but the strongest signals. The A.F. gain control should be adjusted to give the output level required.

When receiving C.W. with the switch at "Manual" the A.F. gain control should be set to maximum gain and the RF/IF control turned down to give a comfortable signal level.

### 6.7 Tuning Meter

The service meter has a switch position marked "Tuning" and with the switch set to this and the A. G.C. on, it may be used as a tuning indicator, the tuning control being adjusted for minimum reading on the meter.
6.8 Muting

When the receiver is used in conjunction with a transmitter, the switch under the meter should be set to one of the muting positions. The muting relay described in para 5.7 will then reduce the gain of the receiver during marks to an extent depending on the setting of the side tone control RI on the muting unit.

### 7.0 MAINTENANCE

### 7.1 Routine Servicing

Routine maintenance of the receiver should be limited to an occasional valve check with the service meter, the replacement of unservicable valves and dial lamps, and the cleaning of contacts as this becomes necessary.

A table of average meter readings is included below and space is left for the recording of the actual readings of the receiver with which this handbook is issued. If, on the routine checks, the reading of a valve is found to have fallen off appreciably, it should be changed and the new reading recorded once it has been ascertained that the change has restored the performance of the receiver to its original level. If this is not the case, then fault finding procedure should be carried out as detailed in para 7.2.
$\mathrm{VI}, 2,3,4$, are reached by removing the centre cover plate over the gang condenser.

V5, 6, 7, By removing the right hand cover over the I.F. unit.

V8, ll, by removing first the tops and then the bodies of the circular screening cans.

V9,10,12, are directly accessible (V12 is very close to mains switch: disconnect mains from power unit before removing)


## NOTE:

The figures given are with no signal input, RF/IF gain control at maximum, and frequency band switch at position E.

Service Meter Readings
Table 3

The three dial lamps fitted to illuminate the scale are connected in parallel with a resistance in series to reduce the current through them. If a lamp fails, unscrew the two pillars securing the dial lamp unit behind the front panel, move the unit away from the dial, replace the faulty lamp and refix the unit into position.

Replacement lamps should be of the 6 volt 0.3 amp miniature Edison screw type. One spare lamp is supplied in a clip fixed to the top of the gang condenser cover inside the receiver.
7.2 Fault Finding

The following procedure should be adopted, should a fault be suspected, and will be of service in locating and correcting the majority of faults met with in operation.
(a) Check the valve currents and H.T. voltage by means of the service meter as indicated in Table 3.
(b) Ascertain whether the fault exists on all frequency ranges. Should it be only on one range, the appropriate oscillator and signal frequency section components and switches should be investigated without further preliminary.
(c) Note any unusual sound effects as these will often give an indication of the trouble.
(d) Make a visual examination for mechanical damage or broken down components.
(e) If a test meter is available, make the voltage and resistance checks indicated in Table 4 below.

Measurements should be made on an Avometer Model 7, the anode and screen potentials on the 400 volt range and the cathode potentials on the 10 volt range. It should be noted that it is necessary to switch the receiver off before making the resistance checks.

| Valves |  | V18.2 | V3 | V4 | V5 | V6 | V7 | V8 | V11 | V12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Anode | Volts to Chassis | 250 | 250 | 95 | 250 | 250 | 250 | 70 | 70 | 270 |
|  | Ohms to H. T. Line | 4.7K | 4.7 K | 4.7K | 4.7K | 4.7K | 4.7K | 122 K | 105K | * |
| Screen | Volts to Chassis | 95 | 104 |  | 95 | 95 | 95 | 45 | 130 | 280 |
|  | $\begin{aligned} & \text { Ohms to } \\ & \text { H.T. Line } \end{aligned}$ | 10K | 4.7 K |  | 10K | 10K | 100K | 100K | 155K | 0 |
| Cathode | Volts to Chassis | 2.4 | 2.4 | 0 | 2.4 | 2.4 | 2.4 | 0 | 4.8 | 18 |
|  | Ohms to Chassis | 330 | 150 | 0 | 330 | 330 | 330 | 0 | 3.3K | 470 |
| Grid | Ohms to Chassis |  |  | 68K |  |  |  | 100K | 100K | 470K |
| Main H.T. 280 volts, Stabilised H.T. 114 volts, H.T. current $\underset{100 \mathrm{~mA}}{\substack{\text { ( }}}$ |  |  |  |  |  |  |  |  |  |  |

* Open circuit when the receiver is in the OFF position. 180 onms when ON. (withdraw the mains plug in order to measure)

Test Point Voltages and Resistances

## Table 4

It is possible that one of the above tests will give an indication of the location of the fault and the appropriate section of the receiver should be investigated. Otherwise, the sections should be tested in order. Details of the tests for the various sections are given below.

### 7.2.1 Power Unit

If no I.T. or H.T. is available from the power unit, check that the mains supply is through to the input plug. Examine the mains fuses on the front
panel and make sure that the primary taps of the transformer are connected correctly. Check the input lead for broken wires.

If the L.T. is available but there is no H.T., examine the fuse F .3 on the front panel. A burnt out fuse indicates a low resistance path to earth from the H.T. line, either in the power unit or the receiver. Test both of the smoothing condensers for breakdown and measure the resistance from the H.T. line to earth. Using an A.C. voltmeter, check the rectifier heater and anode voltages. If these are normal, ( 5 and 365 volts A.C. respectively) the rectifier valve is probably at fault and should be replaced.

The stabilised H.T. supply is nominally 114 volts but if the stabiliser valve is open circuited or making bad contact in the holder, it may be almost 270 volts.

### 7.2.2 Audio Frequency Amplifier

A rapid test of the A.F. amplifier can be made by setting the gain control to maximum and touching the cathode (pin 6) of V1l intermittently with an earthed wire. A loud scatching noise will be produced in the telephone or loudspeaker, if the stage is functioning.

When making tests involving the shorting out of bias resistors, the service meter should be switched to another stage or it may be damaged.

If an audio frequency oscillator is available, the output should be injected into the grids of VI2 and V1l in turn. Lack of response to the former indicates a fault in the output transformer or the leads to it in the interconne cting cable, or in the loudspeaker or telephone. If no response is obtained in the case of V1l, check the coupling condenser and the associated wiring for an open circuit.

### 7.2.3 Intermediate Frequency Amplifier

Again, a rapid test can be made by touching the cathode of the valves V5, V6, and V7, with an earthed wire. The gain controls should be set at maximum for this. If a valve fails to produce any noise, and normal readings are obtained on the test meter, examine the link mechanism to the I.F. changeover switch as this may have slipped (see para 7.3.).

A signal generator and output meter, if available, can be used to measure the gain of each I.F. stage and the results compared with the average set below. The oscillator should not be stopped.

| Valve | $465 \mathrm{kc} / \mathrm{s}$ gain. | $110 \mathrm{kc} / \mathrm{s}$ gain |
| :---: | :---: | :--- |
| V3 | 2 | 1.5 |
| V5 | 15 | 16 |
| V6 | 15 | 16 |

V7 sensitivity
160 mV
100 mV

Sensitivity is given for 2 watts output with a signal modulated at $400 \mathrm{c} / \mathrm{s}$ to a depth of $30 \%$ and the selectivity switch to Posn. 3. This corresponds to $65-70 \mu \mathrm{~A}$ current in the detector diode load R67. If the RF/IF gain control is tested with no aerial connected it will sound noisy due to the very high gain of these circuits. This type of noise should not be confused with that which will arise from a defective gain control.

### 7.2.4 Oscillator

Failure of the oscillator is usually indicated by a rise of anode current and reduced receiver noise although there may be some signal heard. There will be no grid current. The anode current can be checked by means of the service meter while the grid current can be measured by inserting a meter in place of the shorting
link across C 6l. It should be between 60 and 250 ma. Test earth connections and coils for continuity, fixed and variable condensers for short circuits and resistors for incorrect values.

### 7.2.5 Signal Frequency Amplifier and Mixer

Adjust the receiver to the setting for a strong signal and disconnect the aerial from its normal position. Touch it on the grids of V1, V2 and V3 in turn until the signal is heard. The fault lies on the aerial side of this point.

When a signal generator and output meter are available, they can be used to check the performance of each stage and the figures compared with the table given below:

| Range | Frequency | Ae. Gain | V1 Gain | V2 Gain | V3 Sensi fivity in $\mu \mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A | $24 \mathrm{Mc} / \mathrm{s}$ | 6 | 6 | 6 | 320 Bandwidth 4 |
| B | $12 \mathrm{Mc} / \mathrm{s}$ | 5 | 14 | 15 | 400 Bandwidth 4 |
| C | $6 \mathrm{Mc} / \mathrm{s}$ | 9 | 4 | 20 | 400 Bandwidth 4 |
| D | $3 \mathrm{Mc} / \mathrm{s}$ | 9 | 11 | 4.4 | 400 Bandwidth 4 |
| E | $1 \mathrm{Mc} / \mathrm{s}$ | 6 | 4.4 | 24 | 350 Bandwidth 3 |
| F | $425 \mathrm{kc} / \mathrm{s}$ | 1.8 | 6 | 5 | 600 Bandwidth 3 |
| G | $170 \mathrm{kc} / \mathrm{s}$ | 1.8 | 2.5 | 10 | 350 Bandwidth 3 |
| H | $20 \mathrm{kc} / \mathrm{s}$ | 1.8 | 5.6 | 33 | 600 Bandwidth 2 |
| Measured with dummy aerial of 80 ohms above $4 \mathrm{Mc} / \mathrm{s}$ and 300 pF below $4 \mathrm{Mc} / \mathrm{s}$. V3 sensitivity is for 2 watts audio output on $400 \mathrm{c} / \mathrm{s}, 30 \%$ modulated signal. R.F. and A.F. gain controls are at maximum. |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

Signal Amplifier Gains
Table 5

### 7.2.6 A.G.C. and Noise Suppressor

The A.G.C. and noise suppressor operation should be checked in the following manner:-

Set the meter switch to "Tuning".
Set the A.G.C. - N.S. switch to N.S. - A.G.C.
Connect the aerial to the receiver, advance the gain controls, tune in strong carrier wave and note whether the meter reading falls.

Advance noise suppressor control when distortion and attenuation of a modulated carrier should result.

If the A.G.C. does not function correctly, check the continuity of the line from the diode (V9) to the grid return circuit of the R.F. and I.F. valves, including the decoupling resistances. The associated de-coupling condensers should also be tested as a breakdown in one of these would short to earth either the A.G.C. line or one of the valve grid returns.

Examine the switch contacts in the circuits i.e. on the A.G.C. - N.S. switch S.2, and on S.6/6 which effects the I.F. changeover and is mechanically coupled to the wave change switch.

Measure the delay at the cathode of V9 (pin 8). It should be 9 or 10 volts. If it is incorrect, check the values of $R 75$ and 76 which form a potential divider across the H.T.

If the noise suppressor is faulty, check the condensers, resistors and switches in this part of the circuit for breakdown, value and dirty contacts respectively.
7.2.7 Beat Frequency Oscillator

A high anode current reading when V8 is checked on the service meter, usually indicates that the valve is not oscillating and the associated components should be checked. If the valve appears to be oscillating but
the beat note is still inaudible, adjustments to the preset tuning control may be necessary (see para 7.4).
7.3 Mechanical Adjustments.

The switch on the I.F. unit for changing from 110 to $465 \mathrm{kc} / \mathrm{s}$ operation, is rotated by means of an insulated link operated by a cam on the wave band switch shaft. The insulated portion of this link has two slotted holes at one end for adjustment of length. If, for any reason, the I.F. switch is not operating on the correct contacts, slacken the lock nuts and screws on the links, adjust to the correct position and retighten screws and locknuts. It is essential that the bearings of this switch are lubricated, (Microtime Type $C$ is suitable) and this necessitates the removal of the receiver from the housing. The side cover must then be removed to render them accessible.

Should the clutch drive mechanism show a tendency to slip, which is indicated by an apparent sticking of the logging scale, this can be corrected as follows:-

The clutch is located between the dial drive mechanism and the variable condensers, immediately in front of the flexible coupling. Two O.B.A. hexagonal nuts in contact with plain washers at the rear ends of the clutch springs are provided for adjusting the tension. These should be moved about one sixth of a turn at a time until no slip is apparent. iach spring should be adjusted by an equal amount to avoid uneven pressure on the clutch plates.

Replacement of the glass tuning dial should be carried out in the following order, should this become necessary.

Remove the slow motion tuning knob from the main drive spindle by undoing the grub screws.

Remove the main tuning knob by unscrewing the two retaining bolts.

Remove the escutcheon.

The glass dial is held in position by two vertical metal strips, one on each side of the scale. Unscrew the bolts, top and bottom, and remove the strips and rubber packing. Clear out the broken glass and replace with the new scale. Replace the metal holding strips, taking care that the rubber packing is properly in position. Tighten the screws sufficiently to hold the glass in position and replace the main tuning knob.

The dial should now be aligned with the fine logging scale. This is done by obtaining a zero reading on the logging scale when the pointer on the dial lies in each of the following positions:-
a) On the line between 1 and 2 of the coarse logging scale.
b) On the line between 11 and 12.
c) On the line between 22 and 23.

In the extreme positions, a mark will be found near the edge of the dial and the pointer should be lined up on this.

Gently tighten the screws so that the glass is held rigidly in position. Remove the main tuning kmob and replace the escutcheon fastening the former back into position.

### 7.4 Circuit Alignment

No attempt should be made to readjust the preset inductance and capacity trimmers of the receiver unless the appropriate test equipment is available and alignment should be undertaker only by experienced personnel when there is definite evidence that this is required.
I.F. Amplifier and B.F.O.

A signal generator and $0-0.5 \mathrm{~mA}$ meter are required, When aligning the I.F. circuits and if an oscilloscope is available and the generator can be frequency
modulated, it will be easier to obtain symmetry on bandwidths 3, 4 and 5. Unless special D.C. coupled equipment is available with a very low sweep rate, widths 1 and 2 must be checked by setting the signal generator each side of the intermediate frequency and comparing the outputs.

Typical I.F. response curves are given in the appendix and these should be referred to.

Free the I.F. cores with a solvent such as Amyl Acetate or Acetone and conneqt the output of the signal generator to the mixer gride ama the $0-0.5 \mathrm{~mA}$ meter between the bottom of the resistor R 67 and chassis. A deflection of $70 \mu \mathrm{~A}$ should be taken as standard.

## NOTE

The oscillator should not be stopped or the valve removed as this will have a detrimental effect on the mixer valve. The A.G.C. should be switched off and gain controls set at maximum.
$465 \mathrm{kc} / \mathrm{s}$ Channel.
a. Set the range switch to E.
b. Set the bandwidth switch to Posn, 1 and the signal generator to $465 \mathrm{kc} / \mathrm{s}$, trimming the latter for maximum deflection of the meter. This ensures that the generator is set to the crystal resonance frequency.
c. Set the bandwidth switch to Posn. 3 and peak all the channel I.F. transformers except transformers $B$ and $D$.
d. Set the bandwidth switch to Posn. 4 and adjust transformer B for symmetry of response with the oscilloscope across R67 and frequency modulating the generator.
e. Set the bandwidth switch to Posn. 1 and adjust C65 for symmetry of response by rocking the generator frequency each side of the I.F.
f. Set the bandwidth switch to Posn. 2 and adjust L9 and C67 until curve is both single humped and symmetrical in a similar manner.
g. Set the bandwidth switch to Posn. l, the B.F.O. panel control to its central position, check that this corresponds to half capacity and adjust L35 for zero beat on the oscilloscope.

There are two possible positions of the core and the inner one should be chosen.

## $110 \mathrm{kc} / \mathrm{s}$ Channel.

a. Set the range switch to $F$.
b. Set the bandwidth switch to Posn. l, the signal generator to $110 \mathrm{kc} / \mathrm{s}$, and trim the latter for maximum deflection of the meter.
c. Set the bandwidth switch to Posn. 3 and adjust L39 and I40 and then the cores of the transformers $G$ and $J$ between $V 6$ and $V 7$ for maximum response.
d. Unscrew the top cores of the transformers $G$ and $J$ between V5 and V6 and adjust the bottom cores for maximum response.
e. Damp the grid of $V 6$ using a $22 \mathrm{~K} \Omega$ resistor in series with a O.1 $\mu \mathrm{F}$ condenser.
f. Adjust the top core of the $V 6$ anode transformer $J$ for maximum response. Remove the damper.
g. Damp the anode of V 5 and adjust the top core of the anode transformer $G$ for maximum response. Remove the damper.
h. Adjust the top core of the transformer for symmetry by rocking the generator frequency.
i. Set the bandwidth switch to Posn. 4 and adjust the top core of transformer C for symmetry using the oscilloscope. (The dip, which can be seen here, - will be filled by the R.F.response)
j. Set the bandwidth switch to Posn, l and adjust C68 for symmetry by rocking the generator frequency.
k. Set the bandwidth switch to Posn. 2 and adjust Illo for minimum height of peak. Care should be taken to adjust the generator continually to the resonance frequency as this is critical and varies slightly.

1. Set the bandwidth switch to Posn. 5 and adjust C64 for symmetry using the oscilloscope.
m. Set the bandwidth switch to Posn. 1, the B.F.O. panel control to the central position, and adjust L36 for zero beat, choosing the inner position of the core.

Signal Frequency Amplifier and Oscillator.
Each range is aligned separately, first the oscillator, then the two intervalve signal frequency circuits and finally the aerial coils.

The signal generator should be connected to the aerial input via an 80 ohm dummy aerial on bands $A$ to $C$ and via one of 300 pF on the remainder of the bands. The input level should be about 1 mV and the RF/IF gain control should be adjusted to give some $70 \mu A$ current in the diode detector load. This should be measured by the $0-0.5 \mathrm{~mA}$ meter which should be connected between the diode load and earth.

The A.G.C. should be switched off and the gain controls set at maximum. The aerial trimmer should be at half capacity.

BAND A.
a. Set the tuning control $17 \mathrm{Mc} / \mathrm{s}$ on the scale and the bandwidth switch to Posn. 3, Adjust LO 8, IM $8, \mathrm{LR} 8$ and LA 8 for maximum on a $17 \mathrm{Mc} / \mathrm{s}$ signal.
b. Set the tuning control to $31 \mathrm{Mc} / \mathrm{s}$ and adjust $T 08$, TM 8 and $T \mathbb{R}$, for maximum with the appropriate signal.
c. Check that the image frequency lies $0.93 \mathrm{Mc} / \mathrm{s}$ above the correct signal by connecting the generator to the grid of the mixer and taning it for maximum output.
d. Repeat a and b until no improvement can be obtained. The final adjustment should be at $31 \mathrm{Mc} / \mathrm{s}$.

BAND B
a. Set the tuning control to $8.5 \mathrm{Mc} / \mathrm{s}$ on the scale and adjust LO 7, IM 7, LR 7 and LA 7 for maximum on an $8.5 \mathrm{Mc} / \mathrm{s}$ signal.
b. Set the tuning control to $15.5 \mathrm{Mc} / \mathrm{s}$ and adjust TO 7, TM 7 and TR 7 for maximum with the appropriate signal.
c. Repeat a and b until no further improvement can be obtained. The final adjustment should be at 15.5 $\mathrm{Mc} / \mathrm{s}$.

BAND C.
a. Set the tuning control to $4 \mathrm{Mc} / \mathrm{s}$ on the scale and adjust LO 6, LM 6, LR 6 and LA 6 for maximum on a $4 \mathrm{Mc} / \mathrm{s}$ signal.
b. Set the tuning control to $7.8 \mathrm{Mc} / \mathrm{s}$ and adjust $T 06$, TM 6 and $\mathbb{T R} 6$ for maximum on the appropriate signal.
c. Repeat a and $b$ until no further improvement can be obtained. The final adjustment should be at $7.8 \mathrm{Mc} / \mathrm{s}$.

BAND D.
a. Set the tuning control to $1.7 \mathrm{Mc} / \mathrm{s}$ on the scale and adjust LO 5, LM 5, LR 5, and LA 5 for maximum on a $1.7 \mathrm{Mc} / \mathrm{s}$ signal.
b. Set the tuning control to $3.8 \mathrm{Mc} / \mathrm{s}$ and adjust 105 , TM 5, and TR 5 for maximum on the appropriate signal.
c. Set the signal generator to $2.8 \mathrm{Mc} / \mathrm{s}$ and tune the receiver for maximum output. If the scale reading is higher than $2.8 \mathrm{Mc} / \mathrm{s}$ the capacity of padder, PO 5, should be increased slightly. If it is lower, the capacity should be reduced.
d. Repeat a, b and c until no further improvement can be obtained. The final adjustment should be at $3.8 \mathrm{Mc} / \mathrm{s}$.

BAND E.
a. Set the tuning control to 650kc/s on the scale and adjust IO 4, LM 4 IR 4 and IA 4 for maximum on a $650 \mathrm{kc} / \mathrm{s}$ signal.
b. Set the tuning control to $1500 \mathrm{kc} / \mathrm{s}$ and adjust TO 4, TM 4 and TR 4 for maximum on the appropriate signal.
c. Set the signal generator to $1050 \mathrm{kc} / \mathrm{s}$ and tune the receiver for maximum output. If the scale reading is higher than $1050 \mathrm{kc} / \mathrm{s}$, the capacity of the padder PO 4, shoulu be increased slightly. If it is lower, the capacity should be reduced.
d. Repeat $a, b$ and $c$ until no further improvement can be obtained. The final adjustment should be at $1500 \mathrm{kc} / \mathrm{s}$.

## BAND

a. Set the tuning control to $275 \mathrm{kc} / \mathrm{s}$ on the scale and adjust $I 0$ 3, IM 3, IR 3, and IA 3 for maximum on a $275 \mathrm{kc} / \mathrm{s}$ signal.
b. Set the tuning control to $575 \mathrm{kc} / \mathrm{s}$ and adjust $T 0$ 3, TM 3 and TR 3 for maximum on the appropriate signal.
c. Set the signal generator to $425 \mathrm{kc} / \mathrm{s}$ and tune the receiver for maximum output. If. the scale reading is then higher than $425 \mathrm{kc} / \mathrm{s}$, the capacity of the padder, PO 3, should be increased slightly. If it is lower, the capacity should be reduced.
d. Repeat a, b and c until no further improvement can be obtained. The final adjustment should be at $575 \mathrm{kc} / \mathrm{s}$.

BAND G.
a. Set the tuning control to $110 \mathrm{kc} / \mathrm{s}$ and the bandwidth switch to Posn. 2. Adjust IO 2, IM 2, LR 2 and LA 2 for maximum on a $110 \mathrm{kc} / \mathrm{s}$ signal.
b. Set the tuning control to $240 \mathrm{kc} / \mathrm{s}$ and adjust TO 2, TM 2 and $\mathbb{T R} 2$ for maximum on the appropriate signal.
c. Set the signal generator to $170 \mathrm{kc} / \mathrm{s}$, and tune the receiver for maximum output. If the scale reading is then higher than $170 \mathrm{kc} / \mathrm{s}$, the capacity of the padder, PO 2, should be increased slightly. If it is lower, the capacity should be reduced.
d. Repeat $a, b$ and $c$ until no further improvement can be obtained. The final adjustment should be at $240 \mathrm{kc} / \mathrm{s}$.

## BAND H.

a. Set the tuning control to $14 \mathrm{kc} / \mathrm{s}$ on the scale and the bandwidth switch to Posn. 1 . Adjust LO 1 , LM $1, L R 1$ and $L A 1$ for maximum on a $14 \mathrm{kc} / \mathrm{s}$ signal.
b. Set the tuning control to $25 \mathrm{kc} / \mathrm{s}$ and adjust $T O \mathrm{l}$, TM 1 and TR 1 for maximum on the appropriate signal.
c. Set the signal generator to $20 \mathrm{kc} / \mathrm{s}$ and tune the receiver for maximum output. If the scale reading is then higher than $20 \mathrm{kc} / \mathrm{s}$, the capacity of the padder, $P O 1$, should be increased very slightly. If it is lower, the capacity should be reduced. The padder adjustments are extremely critical on this band.
d. Repeat a, b and c until no further improvement can be obtained. The final adjustment should be at $25 \mathrm{kc} / \mathrm{s}$.

## Adjustment of the I.F. Rejectors

Set the signal generator to the exact intermediate frequency by connecting it to the mixer grid and tuning for maximum output with the bandwidth switch to Posn. 1.

Transfer the signal generator to the grid of V1 and adjust the appropriate I.F. rejector for minimum output. A high level of input will be necessary in order to do this.

On range $E$ adjust $L 2$ with the receiver tuning at the high freque..cy end of the scale. On range $G$ adjust I 1 with the tuning at the low frequency end.




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