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MDA3500 Series



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MDA3500 Series



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MDA3500 Series



AMBIENT TEMPERATURE DERATING INFORMATION

FIGURE 10B - IERC HEATSINK UP3 AND NO HEATSINK



TA, AMBIENT TEMPERATURE (°C)

NOTE 3: SPLIT LOAD DERATING INFORMATION

lated as follows:

ambient)

Bridge rectifiers are used in two basic configurations as shown by circuits A and B of Figure 11. The current derating data of Figure 4 applies to the standard bridge circuit (A) where $I_A = I_B$. For circuit B where $I_A = I_B$, derating information can be calcu-

(6) $T_R(M_{ax}) = T_J(M_{ax}) - \Delta T_{J1}$ Where $T_R(M_{ax})$ is the reference temperature (either case or

For example, to determine $T_{C(Max)}$ for the MDA3500 with the following capacitive load conditions.

I_B = 10 A average with a peak of 70 A First calculate the peak to average ratio for I_A. I_(PK)/I_(AV) = 60/10 = 6.0. (Note that the peak to average ratio is on a per diode basis and each diode provides 10 A average). From Figure 5, for an average current of 20 A and an I_(PK)/ I_(AV) = 6.0 read P_{DT}(AV) = 40 watts or 10 watts/diode. Thus P_{D1} = P_{D3} = 10 watts. Similarly, for a load current I_B of 10 A, diode #2 and diode #4 each see 5.0 A average resulting in an I_(PK)/I_(AV) = 10. watts of a performance of the avelage average direction in the avelage for the average for the

Thus, the package power dissipation for 10 A is 20 watts or 5.0 watts/diode $\therefore P_{D2} = P_{D4} = 5.0$ watts. The maximum junction temperature occurs in diode #1 and #3.

The maximum junction temperature occurs in diode #1 and #3. From equation (3) for diode #1 $\Delta T_{J1} = (7.5)$ (10), since coupling is negligible. $\Delta T_{J1} \approx 75^{9}C$ Thus $T_{C(Max)} \approx 175 - 75 = 100^{9}C$ The total package dissipation in this example is: $P_{DT(AV)} = 2 \times 10 + 2 \times 5.0 = 30$ watts, which must be considered when selecting a heat sink.

 ΔT_{J1} can be calculated using equation (3) in Note 2.

 $I_A = 20$ A average with a peak of 60 A $I_B = 10$ A average with a peak of 70 A

NOTE 2: THERMAL COUPLING AND EFFECTIVE THERMAL RESISTANCE

In multiple chip devices where there is coupling of heat between die, the junction temperature can be calculated as follows:

(1) $\Delta T_{J1} = R_{\theta 1} P_{D1} + R_{\theta 2} K_{\theta 2} P_{D2} + R_{\theta 3} K_{\theta 3} P_{D3}$

 $\begin{array}{c} + R_{04} K_{04} P_{D4} \\ \text{Where } ^{T}_{J1} \text{ is the change in junction temperature of diode 1} \\ R_{01} \text{ thru 4 is the thermal resistance of diodes 1 through 4} \\ P_{D1} \text{ thru 4 is the power dissipated in diodes 1 through 4} \end{array}$

 $K_{\theta 2}$ thru 4 is the thermal coupling between diode 1 and diodes 2 through 4.

An effective package thermal resistance can be defined as follows:

(2) $R_{\emptyset}(EFF) = {}^{\Delta}T_{J1}/P_{DT}$ Where: P_DT is the total package power dissipation Assuming equal thermal resistance for each die, equation (1) simplifies to

simplifies to (3) $\Delta T_{J1} = R_{\partial 1} (P_{D1} + K_{\partial 2}P_{D2} + K_{\partial 3}P_{D3} + K_{\partial 4}P_{D4})$ For the conditions where $P_{D1} = P_{D2} = P_{D3} = P_{D4}$, $P_{DT} = 4P_{D1}$, equation (3) can be further simplified and by substituting into equation (2) results in

(4) $R_{\theta}(EFF) = R_{\theta 1} (1 + K_{\theta 2} + K_{\theta 3} + K_{\theta 4})/4$

When the case is used as a reference point, coupling between die is neglegible for the MDA3500. When the bridge is used without www.Data heatink, coupling between die is approximately 70% and Rg1 is 30° C/W,

 $A_{\theta}(EFF) = 30 [1 + (3) (.7)]/4 = 23^{\circ}C/W$



Circuit A





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FIGURE 11- BASIC CIRCUIT USES FOR